# Dynamic Universe Model solves "Faster than Light Neutrinos" riddle. 

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#### Abstract

: There are many instances that reported Superluminal neutrinos. Dynamic Universe Model explains the how and why of "Faster than Light Neutrinos" without any modification in its theory. Various instances like Astronomical jets, Gravitational catapult, MINOS experiment and Fermilab1979 in particle experiments and supernova SN1987A and Gamma Ray Bursts (GRBs) in astronomy Neutrinos travelling faster than speed of light were recorded. There were 76 theoretical experiments conducted and their results are reported in this paper. These experiments were done between 2009 to 2011. Dynamic Universe Model theory was tested in explaining many anomalies in Physics. Dynamic Universe Model's many predictions came true.


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## Key words

Dynamic universe Model; SITA programming; Micro particle world; VLBI Very Long Baseline Interferometry; Gravitational Bending: PPN formulations; Faster than light neutrinos; Super luminous neutrinos;

## 1. Introduction:

"Faster than Light Neutrinos" were observed in Dynamic Universe Model while working with VLBI papers in 2008 or so. That time no further work was done on this front. Now the earlier work was dug-up again for the theoretical evidences after seeing many observational reports of faster than light (or super luminal) neutrinos. The output graphs of all the cases of these 76 different situations were presented in Table 4. Two typical Graphs were presented in the paper where super luminal neutrinos are seen. It can be said that the SITA calculation methods of Dynamic Universe Model can be used without any modifications for explaining "Faster than Light Neutrinos" There are many
experimental verifications, astronomical observations and news items supporting "Faster than light neutrinos" in the literature. There are some which are against. I am not discussing many of them
1.1. Astronomical jets, In January 1999, John Biretta ${ }^{[1]}$ reported HUBBLE DETECTS FASTER-THAN-LIGHT MOTION IN GALAXY M87. They found clouds which appear to move many times faster than the speed of light, shooting out from the Galaxy center region of the M87 galaxy.

### 1.2. MINOS experiment

Autiero of OPERA experiment realized that the same equipment of OPERA can be used for measuring speed of neutrinos and worked out the MINOS experiment. First he published results in $2011^{[2]}$ later this result was contradicted by OPERA director in 2012, and said neutrinos are travelling at the velocity of light.
1.3. Fermilab1979 particle experiments

Zhe Chang, Xin Li, and Sai Wang from Institute of High Energy Physics, China confirmed "superluminal speed formula is consistent with data of OPERA, MINOS and Fermilab-1979 neutrino experiments as well as observations on neutrinos from SN1987a ${ }^{\text {[3] }}$

### 1.4. Neutrinos from Supernova SN1987A

Arnett, W.D. et al. (1989) ${ }^{[4]}$ and Nomoto ${ }^{[5]}$ et al (1987) found that the neutrinos emitted from this Supernova explosion reached earth 3hours earlier than the light. This Supernova was at a distance of 168 kLy . Here the assumption is that the neutrinos and the light were released simultaneously from the explosion of SN1987A and the produced neutrinos arrived few hours earlier.

### 1.5. Gamma Ray Bursts (GRBs) in astronomy

Katsuaki Asano of Japan and Kohta Murase of USA ${ }^{[6]}$ said about EeV Neutrinos in the Afterglow Phase that they have experienced about the relativistic shock often becomes superluminal in 2015.

## 2. Applying Dynamic Universe Model:

Dynamic Universe model can calculate the simultaneous gravitational effect of many gravitating bodies like Sun, planets, local stars etc., while considering their dynamic movements. For this purpose, the original mathematical background of Dynamic Universe Model was extended into micro world about 10 years back. SITA programming was used in this case, for doing so, we will take the setup of solar system as on 01.01.2000@00.00:00 hrs using Helio centric ecliptic xyz values and try sending the
neutrino from different directions i.e., in different solar elongation angle Фmin and trace the path of neutrino. I took 76 different xyz coordinates and different directions for neutrinos with the same status of solar system as on 01.01.2000@00.00:00 hrs. The only change from experiment to experiment is the initial position and direction the neutrino. All these theoretical experiments were designed in such a way, the neutrino goes grazingly near Sun or at the minimum distance from the centre of Sun at the moment of time as on 01.01.2000@00.00:00 hrs precisely. taking into account all the dynamic movements of planets and the their gravitational fields on the fast moving neutrino. Each of these computationally intensive theoretical experiments took a time 15 min at the lowest to 24 hours at the highest, on a recent HP Laptop, depending on the number of iterations. Now let us see what Dynamic Universe Model of Cosmology is...

Dynamic Universe Model explains reason behind such variations. General Relativistic Bending depends on the mass and radius of Sun or the main gravitating body only. Whereas Dynamic Universe Model considers Gravitational effect Sun, Planets, Globular clusters, Milky-way, Local systems etc., and finds the Universal gravitational force vector at that instant of time for that configuration of the Universe.

This new type of Mathematics is different from earlier Newtonian two body problem that used differential equations and Einstein's general theory of relativity that used tensors which in turn unwrap into differential equations. This new Math approach was presented as an invited talk in Conference on "Emerging Areas in Pure \& Applied Mathematics" ${ }^{17}$. This Dynamic Universe Model approach solves many unsolved problems like...

1. Galaxy Disk formation using Dynamic Universe Model (Dense mass) Equations
2. Solution to Missing mass in Galaxies: It proves that there is no missing mass in Galaxy due to circular velocity curves
3. Explains gravity disturbances like Pioneer anomaly, etc.
4. Non-collapsing Large scale mass structures formed when non-uniform density distributions of masses were used
5. Offers Singularity free solutions.
6. Non- collapsing Galaxy structures
7. Solving Missing mass in Galaxies, and it finds reason for Galaxy circular velocity curves....
8. Blue shifted and red shifted Galaxies co-existence...
9. Explains the force behind expansion of universe.
10. Explains the large voids and non-uniform matter densities.
11. Predicts the trajectory of New Horizons satellite.
12. Withstands $10^{5}$ (One Hundred Thousand) times the Normal Jeans swindle test
13. Explaining the Pioneer Anomaly
14. Explaining the formation of Astronomical jets
15. Explaining the high velocities in Astronomical Jets
16. Prediction of "No-dark" matter proved experimentally
17. Near light velocities in Astronomical jets
18. Prediction of Blue shifted Galaxies came true
19. Explaining VLBI (Very long Baseline Interferometry)
20. Energy to mass conversion
21. Explaining super luminal neutrinos

Etc...
Only differences used between the various simulations are in the initial values \& the time steps. The structure of masses is different. In the first 2 cases, approximate values of masses and distances were used. In the third and fourth case, real values of masses and distances for a close approximation were used.

Dynamic universe model is different from Newtonian static model, Einstein's Special \& General theories of Relativity, Hoyle's Steady state theory, MOND, M-theory \& String theories or any of the Unified field theories. It is basically computationally intensive real observational data based theoretical system. It is based on non-uniform densities of matter distribution in space. There is no space time continuum. It uses the fact that mass of moon is different to that of a Galaxy. No negative time. No singularity of any kind. No divide by zero error in any computation/ calculation till today. No black holes, No Bigbang or no many minute Bigbangs. All real numbers are used with no imaginary number. Geometry is in Euclidian space. Some of its earlier results are non-collapsing, non-symmetric mass distributions. It proves that there is no missing mass in Galaxy due to circular velocity curves. It is single closed Universe model. Today we are presenting the results of theoretical experiments conducted 7 years back.

Our universe is not a Newtonian type static universe. There is no Big bang singularity, so the question "What happened before Big bang?" does not arise. Ours is neither an expanding nor contracting universe. It is not infinite but it is a closed finite universe. Our universe is neither isotropic nor homogeneous. It is LUMPY. But it is not empty. It may not hold an infinite sink at the infinity to hold all the energy that is escaped. This is closed universe and no energy will go out of it. Ours is not a steady state universe in the sense, it does not require matter generation through empty spaces. No starting point of time is required. Time and spatial coordinates can be chosen as required. No imaginary time, perpendicular to normal time axis, is required. No baby universes, black holes or warm holes were built in.

This universe exists now in the present state, it existed earlier, and it will continue to exist in future also in a similar way. All physical laws will work at any time and at any place. Evidences for the three dimensional rotations or the dynamism of the universe can be seen in the streaming motions of local group and local cluster. Here in this dynamic universe, both the red shifted and blue shifted Galaxies co-exist simultaneously.

A point to be noted here is that the Dynamic Universe Model never reduces to General relativity on any condition. It uses a different type of mathematics based on Newtonian physics. This mathematics used here is simple and straightforward. As there are no differential equations present in Dynamic Universe Model, the set of equations give single solution in x y z Cartesian coordinates for every point mass for every time step. All the mathematics and the Excel based software details are explained in the three
books published by the author [14, 15, 16] In the first book, the solution to N-body problem-called Dynamic Universe Model (SITA) is presented; which is singularity-free, inter-body collision free and dynamically stable. This is the Basic Theory of Dynamic Universe Model published in 2010 [14]. The second book in the series describes the SITA software in EXCEL emphasizing the singularity free portions. It explains more than 21,000 different equations (2011)[15]. The third book describes the SITA software in EXCEL in the accompanying CD / DVD emphasizing mainly HANDS ON usage of a simplified version in an easy way. The third book contains explanation for 3000 equations instead of earlier 21000 (2011)[16].

SITA solution can be used in many places like currently unsolved applications like Pioneer anomaly at the Solar system level, Missing mass due to Star circular velocities and Galaxy disk formation at Galaxy level etc. Here we are using it for prediction of blue shifted Galaxies.

Dynamic Universe model does NOT depend on speculation. It is based on hard observed facts. I am writing these sentences especially as cosmology is becoming more and more speculative today.

The following table gives basic differences between Bigbang based cosmologies and Dynamic Universe Model

|  | General question <br> answered by any <br> theory (Cosmology <br> condition) ........ | Bigbang based <br> cosmology | Dynamic Universe Model |
| :---: | :---: | :---: | :---: |
| $\mathbf{1}$ | It should say <br> something about the <br> creation of Universe <br> / matter. | Required, In the form of <br> Bigbang Singularity. | Not required, NO Bigbang <br> Singularity, No SINGULARITY |
| $\mathbf{2}$ | It should explain <br> about the expansion <br> of Universe. | Says Universe is <br> expanding, But keeps <br> mum about explaining <br> the force behind <br> expansion. | Says Universe is expanding, <br> But explains the force <br> behind expansion. |
| $\mathbf{3}$ | It should say about <br> the universe closed- <br> ness, | Due to Space-time <br> continuum and <br> curvature. | Due to Classical Physics |


| 5 | Dark matter | Cannot explain missing mass, Concept of UNKNOWN dark matter required to explain many things | Explains missing mass, dark matter NOT required |
| :---: | :---: | :---: | :---: |
| 6 | Dark energy | Concept of UNKNOWN dark energy required to explain many things | NOT required |
| 7 | It should tell about existence of Blue shifted Galaxies | Keeps mum No answer | Blue and red-shifted Galaxies can co-exist |
| 8 | It should explain about universe starting assumptions like uniform density of matter | Uniform density of matter required | Can explain large VOIDs, Based on NON uniform mass densities........ |
| 9 | It should deal correctly with celestial mechanics Like pioneer anomaly | Predicts away from SUN Observed is TOWARDS SUN | Predicts towards SUN as Observed (Important) |
| 10 | It should calculate correctly the Trajectory of New horizons satellite to Pluto. | At present trajectory predictions done using thumb-rules not from any model | Theoretically Calculates Trajectory accurately |

3 Mathematical formulation: Into the Micro world

## 3.a. Original Theoretical formation (Tensor):

Let us assume an inhomogeneous and anisotropic set of N point masses moving under mutual gravitation as a system and these point masses are also under the gravitational influence of other additional systems with a different number of point masses in these different. For a broader perspective, let us call this set of all the systems of point masses as an Ensemble. Let us further assume that there are many Ensembles each consisting of a different number of systems with different number of point masses. Similarly, let us further call a group of Ensembles as Aggregate. Let us further define a

Conglomeration as a set of Aggregates and let a further higher system have a number of conglomerations and so on and so forth.

Initially, let us assume a set of N mutually gravitating point masses in a system under Newtonian Gravitation. Let the $\alpha^{\text {th }}$ point mass has mass $\mathrm{m}_{\alpha}$, and is in position $\mathrm{x}_{\alpha}$. In addition to the mutual gravitational force, there exists an external $\phi_{\text {ext }}$, due to other systems, ensembles, aggregates, and conglomerations etc., which also influence the total force $F_{\alpha}$ acting on the point mass $\alpha$. In this case, the $\phi_{\text {ext }}$ is not a constant universal Gravitational field but it is the total vectorial sum of fields at $\mathrm{x}_{\alpha}$ due to all the external to its system bodies and with that configuration at that moment of time, external to its system of $N$ point masses.
Total Mass of system $=M=\sum_{\alpha=1}^{N} m_{\alpha}$
Total force on the point mass $\alpha$ is $F \alpha$, Let $F_{\alpha \beta}$ is the gravitational force on the $\alpha^{\text {th }}$ point mass due to $\beta^{\text {th }}$ point mass.

$$
\begin{equation*}
F_{\alpha}=\sum_{\substack{\alpha=1 \\ \alpha \neq \beta}}^{N} F_{\alpha \beta}-m_{\alpha} \nabla_{\alpha} \Phi_{e x t}(\alpha) \tag{2}
\end{equation*}
$$

Moment of inertia tensor
Consider a system of N point masses with mass $\mathrm{m}_{\alpha}$, at positions $\mathrm{X}_{\alpha}, \alpha=1,2, \ldots \mathrm{~N}$; The moment of inertia tensor is in external back ground field $\phi_{\text {ext. }}$

$$
\begin{equation*}
I_{j k}=\sum_{\alpha=1}^{N} m_{\alpha} x_{j}^{\alpha} x_{k}^{\alpha} \tag{3}
\end{equation*}
$$

Its second derivative is

$$
\begin{equation*}
\frac{d^{2} I_{j k}}{d t^{2}}=\sum_{\alpha=1}^{N} m_{\alpha}\left(\stackrel{\circ}{x_{j}^{\alpha}} x_{k}^{\alpha}+x_{j}^{\alpha} \stackrel{\circ}{x_{k}^{\alpha}}+x_{j}^{\alpha} \stackrel{\circ}{x_{k}^{\alpha}}\right) \tag{4}
\end{equation*}
$$

The total force acting on the point mass $\alpha$ is and $F$ is the unit vector of force at that place of that component.

$$
\begin{equation*}
F_{j}^{\alpha}=m_{\alpha} x_{j}^{\alpha}=\sum_{\substack{\beta=1 \\ \alpha \neq \beta}}^{N} \frac{G m_{\alpha} m_{\beta}\left(x_{j}^{\beta}-x_{j}^{\alpha}\right) \hat{F}}{\left|x^{\beta}-x^{\alpha}\right|^{3}}-\nabla \Phi_{e x t, j} m_{\alpha} \tag{5}
\end{equation*}
$$

Writing a similar formula for $\mathrm{F}_{\mathrm{k}}^{\alpha}$
$F_{k}^{\alpha}=m_{\alpha} x_{k}^{\alpha}=\sum_{\substack{\beta=1 \\ \alpha \neq \beta}}^{N} \frac{G m_{\alpha} m_{\beta}\left(x_{k}^{\beta}-x_{k}^{\alpha}\right) \hat{F}}{\left|x^{\beta}-x^{\alpha}\right|^{3}}-\nabla \Phi_{e x t, k} m_{\alpha}$

$$
\begin{equation*}
\mathrm{OR}=> \tag{7}
\end{equation*}
$$

$$
\begin{align*}
& x_{j}^{\alpha}=\sum_{\substack{\beta=1 \\
\alpha \neq \beta}}^{N} \frac{G m_{\beta}\left(x_{j}^{\beta}-x_{j}^{\alpha}\right) \hat{F}}{\left|x^{\beta}-x^{\alpha}\right|^{3}}-\nabla \Phi_{e x t} \\
& x_{k}^{\alpha}=\sum_{\substack{\beta=1 \\
\alpha \neq \beta}}^{N} \frac{G m_{\beta}\left(x_{k}^{\beta}-x_{k}^{\alpha}\right)}{\left|x^{\beta}-x^{\alpha}\right|^{3}}-\nabla \Phi_{e x t}  \tag{8}\\
& >
\end{align*}
$$

And =>
Lets define Energy tensor (in the external field $\phi_{\text {ext }}$ )

$$
\begin{align*}
\frac{d^{2} I_{j k}}{d t^{2}}= & 2 \sum_{\alpha=1}^{N} m_{\alpha}\left(x_{j}^{\alpha} x_{k}^{\alpha}\right)+\sum_{\substack{\alpha=1 \\
\alpha \neq \beta}}^{N} \sum_{\substack{\beta=1 \\
\alpha \neq \beta}}^{N} \frac{G m_{\alpha} m_{\beta}\left\{\left(x_{k}^{\beta}-x_{k}^{\alpha}\right) x_{j}^{\alpha}+\left(x_{j}^{\beta}-x_{j}^{\alpha}\right) x_{k}^{\alpha}\right\}}{\left|x^{\beta}-x^{\alpha}\right|^{3}} \\
& -\sum_{\alpha=1}^{N} \nabla \Phi_{e x t} m_{\alpha} x_{j}^{\alpha}-\sum_{\alpha=1}^{N} \nabla \Phi_{e x t} m_{\alpha} x_{k}^{\alpha} \tag{9}
\end{align*}
$$

Lets denote Potential energy tensor $=\mathrm{Wjk}=$
$\sum_{\substack{\alpha=1 \\ \alpha \neq \beta}}^{N} \sum_{\substack{\beta=1 \\ \alpha \neq \beta}}^{N} \frac{G m_{\alpha} m_{\beta}\left\{\left(x_{k}^{\beta}-x_{k}^{\alpha}\right) x_{j}^{\alpha}+\left(x_{j}^{\beta}-x_{j}^{\alpha}\right) x_{k}^{\alpha}\right\}}{\left|x^{\beta}-x^{\alpha}\right|^{3}}$
Lets denote Kinetic energy tensor $=2 \mathrm{~K}_{\mathrm{jk}}=2 \sum_{\alpha=1}^{N} m_{\alpha}\left({ }_{x_{j}^{\alpha}}^{x^{\circ} x_{k}^{\alpha}}\right)$ Lets denote External potential energy tensor $=2 \Phi_{\mathrm{jk}}$
$=\sum_{\alpha=1}^{N} \nabla \Phi_{e x t} m_{\alpha} x_{j}^{\alpha}+\sum_{\alpha=1}^{N} \nabla \Phi_{e x t} m_{\alpha} x_{k}^{\alpha}$
Hence $\frac{d^{2} I_{j k}}{d t^{2}}=W_{j k}+2 K_{j k}-2 \Phi_{j k}$
Here in this case

$$
\begin{align*}
F(\alpha) & =\sum_{\substack{\beta=1 \\
\alpha \neq \beta}}^{N} F_{\alpha \beta}-\nabla \Phi_{\alpha}(\alpha) m_{\alpha}  \tag{13}\\
= & \sum_{\substack{\beta=1 \\
\alpha \neq \beta}}^{N} \frac{G m_{\alpha} m_{\beta}\left(x^{\beta}-x^{\alpha}\right)}{\left|x^{\beta}-x^{\alpha}\right|^{3}}-\nabla \Phi_{e x t} m_{\alpha}  \tag{14}\\
& =\left\{x(\text { int })-\nabla_{\alpha} \Phi_{e x t}(\alpha)\right\} m_{\alpha} \tag{15}
\end{align*}
$$

$$
\begin{equation*}
x(\alpha)=\sum_{\substack{\beta=1 \\ \alpha \neq \beta}}^{N} \frac{G m_{\beta}\left(x^{\beta}-x^{\alpha}\right)}{\left|x^{\beta}-x^{\alpha}\right|^{3}}-\nabla \Phi_{e x t} \tag{16}
\end{equation*}
$$

We know that the total force at $x(\alpha)=F_{\text {tot }}(\alpha)=-\nabla_{\alpha} \Phi_{t o t}(\alpha) m_{\alpha}$ Total PE at $\alpha=m_{\alpha} \Phi_{t o t}(\alpha)=-\int F_{t o t}(\alpha) d x$
$=-\int\left\{\sum_{\substack{\beta=1 \\ \alpha \neq \beta}}^{N} x_{\text {int }}^{\circ \circ \alpha} m_{\alpha}-\nabla_{\alpha} \Phi_{e x t}(\alpha) m_{\alpha}-\right\} d x$
$=\int \sum_{\substack{\beta=1 \\ \alpha \neq \beta}}^{N} \frac{G m_{\beta} m_{\alpha}\left(x^{\beta}-x^{\alpha}\right)}{\left|x^{\beta}-x^{\alpha}\right|^{3}} d x-\int \nabla \Phi_{e x t} m_{\alpha} d x$
Therefore total Gravitational potential $\phi_{\text {tot }}(\alpha)$ at $x(\alpha)$ per unit mass

$$
\begin{equation*}
\Phi_{t o t}(\alpha)=\Phi_{e x t}-\sum_{\substack{\beta=1 \\ \alpha \neq \beta}}^{N} \frac{G m_{\beta}}{\left|x^{\beta}-x^{\alpha}\right|} \tag{17}
\end{equation*}
$$

## Lets discuss the properties of $\phi_{\text {ext }}$ :-

$\phi_{\text {ext }}$ can be subdivided into 3 parts mainly $\phi_{\text {ext }}$ due to higher level system, $\phi_{\text {ext }}$-due to lower level system, $\phi_{\text {ext }}$ due to present level. [ Level : when we are considering point mass in the same system (Galaxy) it is same level, higher level is cluster of galaxies, and lower level is planets \& asteroids].
$\phi_{\text {ext }}$ due to lower levels : If the lower level is existing, at the lower level of the system under consideration, then its own level was considered by system equations. If this lower level exists anywhere outside of the system, center of (mass) gravity outside systems (Galaxies) will act as unit its own internal lower level practically will be considered into calculations. Hence consideration of any lower level is not necessary.

## SYSTEM - ENSEMBLE:

Until now we have considered the system level equations and the meaning of $\phi_{\text {ext. }}$ Now let's consider an ENSEMBLE of system consisting of $\mathrm{N}_{1}, \mathrm{~N}_{2} \ldots$ Njpoint masses in each. These systems are moving in the ensemble due to mutual gravitation between them. For example, each system is a Galaxy, and then ensemble represents a local group. Suppose number of Galaxies is j, Galaxies are systems with point masss N1, N2 ....NJ, we will consider $\phi_{\text {ext }}$ as discussed above. That is we will consider the effect of only higher level system like external Galaxies as a whole, or external local groups as a whole.
Ensemble Equations (Ensemble consists of many systems)

$$
\begin{equation*}
\frac{d^{2} I^{\gamma}{ }_{j k}}{d t^{2}}=W_{j k}^{\gamma}+2 K_{j k}^{\gamma}-2 \Phi_{j k}^{\gamma} \tag{18-E}
\end{equation*}
$$

Here ${ }^{\vee}$ denotes Ensemble.
This $\Phi^{r} \mathrm{jk}$ is the external field produced at system level. And for system

$$
\begin{equation*}
\frac{d^{2} I_{j k}}{d t^{2}}=W_{j k}+2 K_{j k}-2 \Phi_{j k} \tag{13}
\end{equation*}
$$

Assume ensemble in a isolated place. Gravitational potential $\phi_{\text {ext }}(\alpha)$ produced at system level is produced by Ensemble and $\quad \phi^{\gamma}$ ext $(\alpha)=0$ as ensemble is in a isolated place.
$\Phi_{\text {tot }}^{\gamma}(\alpha)=\Phi_{e x t}^{\gamma}-\sum_{\substack{\beta=\neq \beta \\ \alpha \neq \beta}}^{N^{\gamma}} \frac{G m^{\gamma}}{x^{\gamma \beta}-x^{\gamma \alpha} \mid}$
As Ensemble situated in an isolated place, Gravitational potential $\phi^{\vee}$ ext $(\alpha)=0$ There fore

$$
\begin{align*}
& \Phi_{\text {tot }}^{\gamma}=\Phi_{e x t}(\alpha)=-\sum_{\substack{\beta=1 \\
\alpha \neq \beta}}^{N^{\gamma}} \frac{G m_{\beta}^{\gamma}}{\left|x^{\gamma \beta}-x^{\gamma \alpha}\right|}  \tag{20}\\
& \text { And } 2 \Phi_{j k}=-\frac{d^{2} I_{j k}}{d t^{2}}+W_{j k}+2 K_{j k} \tag{13}
\end{align*}
$$

$=\sum_{\alpha=1}^{N} \nabla \Phi_{e x t} m_{\alpha} x_{j}^{\alpha}+\sum_{\alpha=1}^{N} \nabla \Phi_{e x t} m_{\alpha} x_{k}^{\alpha}$

## AGGREGATE Equations(Aggregate consists of many Ensembles )

$$
\frac{d^{2} I_{j k}^{\delta \gamma}}{d t^{2}}=W_{j k}^{\delta \gamma}+2 K_{j k}^{\delta \gamma}-2 \Phi_{j k}^{\delta \gamma}
$$

Here ${ }^{\delta}$ denotes Aggregate.
This $\Phi^{\delta \gamma}{ }^{\delta \mathrm{j} k}$ is the external field produced at Ensemble level. And for Ensemble

$$
\begin{equation*}
\frac{d^{2} I^{\gamma}{ }_{j k}}{d t^{2}}=W_{j k}^{\gamma}+2 K_{j k}^{\gamma}-2 \Phi_{j k}^{\gamma} \tag{18-E}
\end{equation*}
$$

Assume Aggregate in an isolated place. Gravitational potential $\phi_{\text {ext }}(\alpha)$ produced at Ensemble level is produced by Aggregate and $\phi^{\delta \gamma}{ }_{\text {ext }}(\alpha)=0$ as Aggregate is in a isolated place.
$\Phi_{\text {tot }}^{\delta,}(\alpha)=\Phi_{e t t}^{\delta \gamma}-\sum_{\substack{\beta=1 \\ \alpha \neq \beta}}^{N^{\delta \gamma}} \frac{G m_{\beta}^{\delta \gamma}}{\left|x^{\delta / \beta}-x^{\delta / \alpha}\right|}$

$$
\begin{equation*}
\Phi_{\text {tot }}^{\delta \gamma}\left(\text { Aggregate } \text { ) }=\Phi_{\text {ett }}^{\gamma}(\alpha)(\text { Ensemble })=-\sum_{\substack{\beta=1 \\ \alpha \neq \beta}}^{N^{\delta \gamma}} \frac{G m_{\beta}^{\delta \gamma}}{\left|x^{\delta / \beta}-x^{\delta, \alpha}\right|}\right. \tag{22}
\end{equation*}
$$

Therefore

## Total AGGREGATE Equations :( Aggregate consists of many Ensembles and systems)

Assuming these forces are conservative, we can find the resultant force by adding separate forces vectorially from equations (20) and (23).

$$
\begin{equation*}
\Phi_{e x t}(\alpha)=-\sum_{\substack{\beta=1 \\ \alpha \neq \beta}}^{N^{\gamma}} \frac{G m_{\beta}^{\gamma}}{\left|x^{\gamma \beta}-x^{\gamma \alpha}\right|}-\sum_{\substack{\beta=1 \\ \alpha \neq \beta}}^{N^{\nu}} \frac{G m_{\beta}^{\delta \gamma}}{\left|x^{\delta, \beta}-x^{\delta, \alpha}\right|} \tag{25}
\end{equation*}
$$

This concept can be extended to still higher levels in a similar way.

## Corollary 1:

$\frac{d^{2} I_{j k}}{d t^{2}}=W_{j k}+2 K_{j k}-2 \Phi_{j k}$
The above equation becomes scalar Virial theorem in the absence of external field, that is $\phi=0$ and in steady state,
i.e. $\begin{aligned} & \frac{d^{2} I_{j k}}{d t^{2}}=0 \\ & 2 K+W=0\end{aligned}$

But when the N -bodies are moving under the influence of mutual gravitation without external field then only the above equation (28) is applicable.

## Corollary 2:

Ensemble achieved a steady state,
i.e. $\frac{d^{2} I_{j k}^{\gamma}}{d t^{2}}=0$

$$
\begin{equation*}
W_{j k}^{\gamma}+2 K_{j k}^{\gamma}=2 \Phi_{j k}^{\gamma} \tag{30}
\end{equation*}
$$

This $\Phi j k$ external field produced at system level. Ensemble achieved a steady state; means system also reached steady state.
i.e. $\frac{d^{2} I_{j k}}{d t^{2}}=0$

$$
\begin{equation*}
W_{j k}+2 K_{j k}=2 \Phi_{j k}^{\gamma} \tag{27}
\end{equation*}
$$

Equation (20) gives $\phi^{\gamma}$ tot $(\alpha)$, that is external potential field present at the system level. Combining Eqn (31) and eqn (9).
$2 \Phi_{e x t} j k=\sum_{\alpha=1}^{N} \nabla \Phi_{e x t} m_{\alpha} x_{j}^{\alpha}+\sum_{\alpha=1}^{N} \nabla \Phi_{e x t} m_{\alpha} x_{k}^{\alpha}$

The Equation 25 is the main powerful equation, which gives many results that are not possible otherwise today. This tensor can be subdivided into 21000 small equations without any differential equations or integral equations. Hence, this set up gives a unique solution of Cartesian X, Y, Z components of coordinates, velocities and accelerations of each point mass in the setup for that particular instant of time. A point to be noted here is that the Dynamic Universe Model never reduces to General relativity on any condition. It uses a different type of mathematics based on Newtonian physics. This mathematics used here is simple and straightforward. All the mathematics and the Excel based software details are explained in the three books published by the author ${ }^{14,}$ 15, 16

Now let's see how the Dynamic Universe Model extends into Micro world mathematically.

## 3.b. Additional mathematical formulation allowing for the Micro world:

In addition to previously published mathematical formulation (viz. eqn 1 to 31) for Dynamic Universe Model, as cited in section 3, the following new equations are added to enable this model for operating into Micro world.
Combining both 3 and 25 (Newly introduced in this paper)

$$
\begin{equation*}
F_{\alpha}=\sum_{\substack{\alpha=1 \\ \alpha \neq \beta}}^{N} F_{\alpha \beta}-m_{\alpha} \nabla_{\alpha}\left[-\sum_{\substack{\beta=1 \\ \alpha \neq \beta}}^{N^{\gamma}} \frac{G m_{\beta}^{\gamma}}{\left|x^{\gamma \beta}-x^{\gamma \alpha}\right|}-\sum_{\substack{\beta=1 \\ \alpha \neq \beta}}^{N^{\delta \gamma}} \frac{G m_{\beta}^{\delta \gamma}}{\left|x^{\delta / \beta}-x^{\delta \gamma \alpha}\right|}\right] \tag{32}
\end{equation*}
$$

So ...

$$
\begin{equation*}
F_{\alpha}=\sum_{\substack{\alpha=1 \\ \alpha \neq \beta}}^{N} F_{\alpha \beta}+m_{\alpha} \nabla_{\alpha}\left[\sum_{\substack{\beta=1 \\ \alpha \neq \beta}}^{N^{\gamma}} \frac{G m_{\beta}^{\gamma}}{\left|x^{\gamma \beta}-x^{\gamma \alpha}\right|}+\sum_{\substack{\beta=1 \\ \alpha \neq \beta}}^{N^{\delta \gamma}} \frac{G m_{\beta}^{\delta \gamma}}{\left|x^{\delta \gamma \beta}-x^{\delta \gamma \alpha}\right|}\right] \tag{33}
\end{equation*}
$$

Interchanging $\sum$ and $\nabla$ operations:

$$
\begin{equation*}
F_{\alpha}=\sum_{\substack{\alpha=1 \\ \alpha \neq \beta}}^{N} F_{\alpha \beta}+m_{\alpha}\left[\sum_{\substack{\beta=1 \\ \alpha \neq \beta}}^{N^{\gamma}} \nabla_{\alpha} \frac{G m_{\beta}^{\gamma}}{\left|x^{\gamma \beta}-x^{\gamma \alpha}\right|}+\sum_{\substack{\beta=1 \\ \alpha \neq \beta}}^{N^{\delta \gamma}} \nabla_{\alpha} \frac{G m_{\beta}^{\delta \gamma}}{\left|x^{\delta \gamma \beta}-x^{\delta \gamma \alpha}\right|}\right] \tag{34}
\end{equation*}
$$

Or
$F_{\alpha}=\sum_{\substack{\alpha=1 \\ \alpha \neq \beta}}^{N} F_{\alpha \beta}+\sum_{\substack{\beta=1 \\ \alpha \neq \beta}}^{N^{\gamma}} \nabla_{\alpha} \frac{G m_{\alpha} m_{\beta}^{\gamma}}{\left|x^{\gamma \beta}-x^{\gamma \alpha}\right|}+\sum_{\substack{\beta=1 \\ \alpha \neq \beta}}^{N^{\delta \gamma}} \nabla_{\alpha} \frac{G m_{\alpha} m_{\beta}^{\delta \gamma}}{\left|x^{\delta / \beta}-x^{\delta / \alpha}\right|}$
The above equation 35 means the force on $a^{\text {th }}$ point mass will be a sum of three components i.e., the summation of attraction forces due to point masses from its own system, ensemble and aggregate. This is the key result that can be applied to point masses or subatomic particles or can be combined in any fashion together. The equations 34 \& 35 are important, simple \& straightforward results.

Let us apply the above equations to some practical situations like radio waves that are going grazingly near Sun from an artificial satellite and are coming to Earth (VLBI). Let us use SITA algorithm for calculation.

## 4. Initial Values

## Initial value of Mass of neutrino

The basic behavior that a neutrino can oscillate from one flavor to another requires that it must have a mass by Super-Kamiokande (1998) ${ }^{[52]}{ }^{[53]}$ and by KamLAND (2005) ${ }^{[54]}$ ${ }^{[55]}$. The present neutrino mass estimates are between 0.2 eV and 2 eV . Conversion from eV to kg was done using the equation : $(1 \mathrm{eV}) / \mathrm{c}^{2}=\mathrm{x} \mathrm{kg} \mathrm{x}=\left\{\mathrm{e} / \mathrm{c}^{2}\right\}$. Value of conversion factor: $x=1.782661907(11) \times 10^{-36}$.

Here in this paper the particle mass was taken as $1.1 \mathrm{e}-52 \mathrm{~kg}$ which is much smaller than Neutrino mass $=1.5 \mathrm{ev} / \mathrm{c} 2=2.685 \mathrm{e}-36 \mathrm{~kg}$ or Radio wave photon mass $=9.019$ e -46 kg etc. The behaviour shown by such a mass will be experienced by higher mass also. Every mass behave in the similar way in Dynamic Universe Model.

## Initial Values table and other tables

Full set of initial values are shown in Table 1 at the end of this paper. This Table 1 gives the initial values of all the point masses, their respective masses in Kg , and their x y z

Cartesian positions. The summary of all the 76 experiments conducted \& reported in Table 2, which is also at the end of this paper and can be seen in 13 columns. The various filenames, Time step values, Number of iterations, initial position, and final position of the Neutrino, General relativistic deflection (bending) angle, Calculated Solar elongation angle in degrees, and SITA Deflection are mentioned there in 13 columns. But it was condensed from the Table 3. There are 71 columns from where these 13 columns were taken. So the summary and finer differences between each experiment can be found from main Table 3 easily. This Table 3 is uploaded into web along with main file. [The name of the file is 'Vak Table 3 Results 71 columns.xls'; brief description of material: There are 76 data records of final data for each file in 71 columns in a single Excel sheet. The header rows for all the data is in the $3^{\text {rd }}$ and $4^{\text {th }}$ rows. ]."

As a result of SITA calculations, there is an assortment of xyz positions, velocities and accelerations in all iterations at each time step for every one of the 133 point masses. It is possible to track any one of these values for every time step throughout the experiment as needed. This data is in an XLS file and uploaded in Web. The Table 4 contains all the individual iteration outputs for each of the 76 experiments are in an XLS file and uploaded along with the main paper for keeping in e-publication. The summary of each experiment is given in that Excel file web attachment because the large volume of data, which will be given in the web version of this paper. Name of the file is 'Vak Table 4 Consolidation Super luminal neutrino Results.xIs'. Brief description of material : Main Data file: There are 19681 lines in this file in 55 columns. The file is subdivided into as many as 76 sections in a single sheet, instead of 76 separate files. It was thought handling separate 76 files will be very difficult, and the server also many not have provisions to hold that many additional files while uploading. The first file name will start in A2 cell, later the header row for the columns. The data is then follows after a blank row. There will be additional blank rows before the next file data. Each data set varies in number of data rows depending on number of iterations. Each row represents a set of data for that time step. Number of data rows from file to file varies from 40 to 3000. Any further additional details can be obtained by contacting the author. ]." All these tables are available in the webpage ${ }^{[10]}$ which can be down loaded.

These experiments were originally designed to study the solar gravitational bending effects at the planetary positions as on 01.01.2000@00.00:00 hrs on a light neutrino positioned at various locations in solar system. Later the results were grouped to view the with respect to solar elongation angle.

## 4. Super Luminal Neutrinos:

There are 52 cases out of 76 experiments that gave Super luminal neutrinos. For every experiment the initial data like starting position and final position of the neutrino were available in Table 2. Additional details are available in table 3 \& 4. A maximum of about $1200 \mathrm{~m} / \mathrm{s}$ higher neutrinos velocities above velocity of light were observed. These results vary from case to case. Sometimes the peek came to as low as 0.1 meters higher velocity only.

## 5. Results

Two typical graphs are given below. For all the remaining graphs see the Table 4. All the graphs (both the Super Luminal neutrino and normal neutrino cases) are shown in Table 4. For this Fig 1 and 2 the initial conditions are given in the captions of the figures. Number of iterations are 80 for the case fig1, and 1200 for the case of fig 2. Remaining 50 cases of Super luminal 24 cases of normal neutrinos are documented in table 4 , which is a supplementary file for this paper.


Fig1. Super luminal Neutrino initial conditions: Velocities in meters per second (vx, vy, $\mathrm{vz})=(-74948114.5,-280430167.2,-74948114.5)$ and Positions in meters (sx, sy, $\mathrm{sz})=(0, \quad 696001492.1, \quad 0)$. The maximum Neutrino velocity achieved in this case is about $1200 \mathrm{~m} / \mathrm{s}$ higher than the velocity of light


Fig2. Super luminal Neutrino initial conditions: Velocities in meters per second (vx, vy, $\mathrm{vz})=(150.1563894,-211985280,-211985280)$ and Positions in meters (sx, sy, sz) = (696011352, 2804642125, 2804642125). The maximum Neutrino velocity achieved in this case is about $550 \mathrm{~m} / \mathrm{s}$ higher than the velocity of light

One may feel it is very silly to consider the gravitational effect of the entire Universe at that point at that time, the gravitational effect of all the other bodies can be neglected near some huge Gravitating body. No, that is not true. For especially very low weight bodies like Photons of radio waves or light waves, or Neutrinos. Let's see an example. Consider me standing on this earth. One may think gravitation of other bodies like Sun and Moon can be neglected on earth. But what about the tide caused by Sun and Moon in Oceans? Yes it is High tide and Low tide in the morning and evening, or on full-moonday on no-moon-day. And there will be higher tide on a full-moon-day evening. These tides are caused by Gravitation of Sun and Moon only.

Here in Dynamic Universe Model an attempt is made to calculate the 3 dimensional Cartesian vectorial force of Universe approximated to 133 mutually Gravitating Nbodies. These preliminary attempts are giving sufficiently accurate results otherwise not possible by other theories. Of course approximating the Universe by 133 bodies may not be correct and accurate. But these approximations are better than single point mass or uniform mass density approximations. But one has to consider that there are many images present in the Universe for many Galaxies. There are limitations like presently available commercial PCs and their available scientific and mathematical software, their accuracies, with in my purse. The present SITA calculations are giving sufficiently accurate results.

## 6. Conclusion:

A process similar to this happens at stars, Galaxy centers, Astronomical jets etc. Hence we can say Dynamic Universe Model can successfully solve the riddle of "Super Luminal Neutrinos" along with many other problems.

## 7. Acknowledgements:

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See for various maps of Universe and Fig 8 at: http://www.astro.princeton.edu/universe/
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Xxxxx

Table 1:

| SI.No. | Name | Mass (kg) | HELIO CENTRIC ECLIPTIC XYZ VALUES of positions as on 01.01.2000@00.00:00 hrs in METR |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | xecliptic | yecliptic | zecliptic |
| 1 | Particle mass << neutrino mass (The initial Position vary with experiment) | 1.10E-52 | 200000000 | 696000000 | 650947504.6 |
| 2 | Mercury | $3.30 \mathrm{E}+23$ | $\begin{aligned} & 5064417926 \\ & 3 \end{aligned}$ | 8540296134 | -3949485753 |
| 3 | Venus | 4.87E+24 | $\begin{aligned} & 6965787886 \\ & 2 \end{aligned}$ | $\begin{array}{\|l} \hline 8261419807 \\ 9 \end{array}$ | -2889306238 |
| 4 | Earth | 5.97E+24 | $\begin{aligned} & 2956578581 \\ & 8 \\ & \hline \end{aligned}$ | $1.44096 \mathrm{E}+11$ | $2869446.398$ |
| 5 | Mars | $6.42 \mathrm{E}+23$ | -3275068912 | 2.17902E+11 | -4484946284 |
| 6 | Jupiter | $1.90 \mathrm{E}+27$ | 4.09177E+11 | $6.46362 \mathrm{E}+11$ | -6473185584 |
| 7 | Saturn | $5.68 \mathrm{E}+26$ | $1.35874 \mathrm{E}+12$ | 3.39522E+11 | $\begin{aligned} & 4816746141 \\ & 2 \end{aligned}$ |
| 8 | Uranus | 8.68E+25 | $2.97521 \mathrm{E}+12$ | $4.32376 \mathrm{E}+11$ | $\begin{array}{\|l} 4014152547 \\ 7 \\ \hline \end{array}$ |
| 9 | Neptune | $1.02 \mathrm{E}+26$ | $3.61461 \mathrm{E}+12$ | $2.66852 \mathrm{E}+12$ | $\begin{array}{\|l} 2835029013 \\ 8 \\ \hline \end{array}$ |
| 10 | Pluto | $1.27 \mathrm{E}+22$ | $\begin{aligned} & 6931588227 \\ & 3 \end{aligned}$ | $4.69858 \mathrm{E}+12$ | 4.82751E+11 |
| 11 | Moon | $7.35 \mathrm{E}+22$ | $\begin{array}{\|l} 2919165734 \\ 4 \\ \hline \end{array}$ | $1.43975 \mathrm{E}+11$ | 16609650.17 |
| 12 | SUN | 1.99E+30 | 0 | 0 | 0 |
| 13 | near star | $\begin{aligned} & \hline 3.97658 \mathrm{E}+2 \\ & 9 \\ & \hline \end{aligned}$ | $3.07379 \mathrm{E}+16$ | $2.48085 \mathrm{E}+16$ | $5.99014 \mathrm{E}+15$ |
| 14 | near star | $\begin{array}{\|l\|} \hline 1.88888 \mathrm{E}+3 \\ 0 \end{array}$ | $1.70141 \mathrm{E}+16$ | $4.49612 \mathrm{E}+13$ | $3.79378 \mathrm{E}+16$ |
| 15 | near star | $\begin{array}{\|l} \hline 2.18712 \mathrm{E}+3 \\ 0 \\ \hline \end{array}$ | $1.71774 \mathrm{E}+16$ | $1.53305 \mathrm{E}+14$ | 3.78638E+16 |
| 16 | near star | $\begin{array}{\|l} \hline 7.95317 \mathrm{E}+2 \\ 9 \end{array}$ | - $1.85801 \mathrm{E}+15$ | 1.6393E+15 | $5.61485 \mathrm{E}+16$ |


| 17 | near star | $\begin{aligned} & \hline 8.94731 \mathrm{E}+2 \\ & 9 \\ & \hline \end{aligned}$ | $9.02924 \mathrm{E}+15$ | $7.13182 \mathrm{E}+15$ | $7.77879 \mathrm{E}+16$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 18 | near star | $\begin{aligned} & 1.73976 \mathrm{E}+3 \\ & 1 \end{aligned}$ | -3.1682E+16 | $2.99664 \mathrm{E}+16$ | $6.86968 \mathrm{E}+16$ |
| 19 | near star | $\begin{aligned} & \hline 8.94731 \mathrm{E}+2 \\ & 9 \end{aligned}$ | $2.37665 \mathrm{E}+16$ | $7.07555 \mathrm{E}+15$ | $8.82862 \mathrm{E}+16$ |
| 20 | near star | $\begin{aligned} & 1.88888 E+3 \\ & 0 \end{aligned}$ | $9.77757 \mathrm{E}+16$ | $1.69837 \mathrm{E}+16$ | $3.32855 \mathrm{E}+15$ |
| 21 | near star | $\begin{aligned} & 8.94731 \mathrm{E}+2 \\ & 9 \end{aligned}$ | $1.75629 \mathrm{E}+16$ | -2.0874E+16 | $9.78004 \mathrm{E}+16$ |
| 22 | near star | $\begin{array}{\|l\|} \hline 3.97658 \mathrm{E}+2 \\ 9 \end{array}$ | 3.82107E+16 | $6.00795 E+16$ | 7.44241E+16 |
| 23 | near star | $\begin{aligned} & 1.82923 E+3 \\ & 0 \end{aligned}$ | $4.50486 \mathrm{E}+16$ | $3.01003 E+16$ | $9.28066 \mathrm{E}+16$ |
| 24 | near star | $\begin{aligned} & 3.28068 \mathrm{E}+3 \\ & 0 \end{aligned}$ | $8.42312 \mathrm{E}+15$ | $5.24915 \mathrm{E}+16$ | $9.39112 \mathrm{E}+16$ |
| 25 | near star | $\begin{aligned} & 1.19298 E+3 \\ & 0 \end{aligned}$ | $4.60396 \mathrm{E}+16$ | $3.03873 E+16$ | 9.29744E+16 |
| 26 | near star | $\begin{aligned} & 7.95317 E+2 \\ & 9 \end{aligned}$ | $4.90495 \mathrm{E}+16$ | $9.64605 E+16$ | 7.35909E+15 |
| 27 | near star | $\begin{array}{\|l} \hline 8.94731 E+2 \\ 9 \end{array}$ | $4.99158 \mathrm{E}+16$ | $9.78689 \mathrm{E}+16$ | 7.06783E+15 |
| 28 | near star | $\begin{aligned} & \text { 7.95317E+2 } \\ & 9 \end{aligned}$ | $1.39114 \mathrm{E}+16$ | $1.09124 \mathrm{E}+17$ | $4.36506 \mathrm{E}+15$ |
| 29 | near star | $\begin{array}{\|l} \hline 1.82923 \mathrm{E}+3 \\ 0 \\ \hline \end{array}$ | $6.28738 \mathrm{E}+16$ | $8.89396 \mathrm{E}+16$ | $2.56335 \mathrm{E}+16$ |
| 30 | near star | $\begin{array}{\|l\|} \hline 2.18712 \mathrm{E}+3 \\ 0 \end{array}$ | $6.90623 \mathrm{E}+16$ | $8.50246 \mathrm{E}+16$ | $2.58319 \mathrm{E}+16$ |
| 31 | near star | $\begin{aligned} & 3.97658 \mathrm{E}+2 \\ & 9 \end{aligned}$ | $2.35768 \mathrm{E}+16$ | $2.08864 \mathrm{E}+16$ | 1.10275E+17 |
| 32 | near star | $\begin{array}{\|l} \hline 7.95317 \mathrm{E}+2 \\ 9 \end{array}$ | 1.86257E+16 | $5.54342 \mathrm{E}+16$ | $1.01576 \mathrm{E}+17$ |
| 33 | near star | $\begin{array}{\|l\|} \hline 8.94731 \mathrm{E}+2 \\ 9 \\ \hline \end{array}$ | $5.04468 \mathrm{E}+16$ | 3.78032E+16 | $1.03142 \mathrm{E}+17$ |
| 34 | near star | $\begin{aligned} & \hline 1.19298 \mathrm{E}+3 \\ & 0 \\ & \hline \end{aligned}$ | $2.09805 \mathrm{E}+16$ | $4.31965 \mathrm{E}+16$ | $1.11915 \mathrm{E}+17$ |
| 35 | near star | $\begin{aligned} & \hline 5.96488 \mathrm{E}+2 \\ & 9 \end{aligned}$ | $3.34107 \mathrm{E}+16$ | $3.81344 \mathrm{E}+16$ | 1.12791E+17 |
| 36 | near star | $\begin{aligned} & \hline 5.96488 \mathrm{E}+2 \\ & 9 \end{aligned}$ | 1.20105E+17 | - $5.23499 E+15$ | $4.10595 \mathrm{E}+16$ |
| 37 | near star | $\begin{aligned} & 8.94731 \mathrm{E}+2 \\ & 9 \\ & \hline \end{aligned}$ | $5.81398 \mathrm{E}+16$ | 4.54439E+16 | $1.08443 \mathrm{E}+17$ |
| 38 | near star | $\begin{aligned} & \hline 6.95902 \mathrm{E}+2 \\ & 9 \end{aligned}$ | $1.07352 \mathrm{E}+17$ | $7.50846 \mathrm{E}+16$ | -1.2264E+16 |
| 39 | near star | $\begin{aligned} & 9.94146 \mathrm{E}+2 \\ & 9 \end{aligned}$ | $2.96095 \mathrm{E}+16$ | $1.22996 \mathrm{E}+17$ | $4.58116 \mathrm{E}+16$ |


| 40 | near star | $\begin{aligned} & 2.90291 \mathrm{E}+3 \\ & 0 \end{aligned}$ | $8.24904 \mathrm{E}+16$ | $2.35538 \mathrm{E}+16$ | $1.05478 \mathrm{E}+17$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 41 | near star | $\begin{aligned} & 8.94731 E+2 \\ & 9 \end{aligned}$ | $6.10305 \mathrm{E}+16$ | 4.80435E+16 | $1.15415 \mathrm{E}+17$ |
| 42 | near star | $\begin{aligned} & 8.94731 \mathrm{E}+2 \\ & 9 \end{aligned}$ | $9.76996 \mathrm{E}+16$ | $2.14625 E+16$ | $9.75422 \mathrm{E}+16$ |
| 43 | near star | $\begin{array}{\|l} \hline 7.95317 \mathrm{E}+2 \\ 9 \end{array}$ | $2.15194 \mathrm{E}+16$ | $1.34558 \mathrm{E}+17$ | $3.20268 \mathrm{E}+16$ |
| 44 | near star | $\begin{array}{\|l} \hline 5.64675 \mathrm{E}+3 \\ 0 \\ \hline \end{array}$ | $5.35209 \mathrm{E}+16$ | $2.81642 \mathrm{E}+16$ | $1.29127 \mathrm{E}+17$ |
| 45 | near star | $\begin{array}{\|l\|} \hline 6.95902 \mathrm{E}+2 \\ 9 \\ \hline \end{array}$ | 1.14625E+16 | 1.39712E+16 | $1.43945 \mathrm{E}+17$ |
| 46 | near star | $\begin{aligned} & 8.94731 \mathrm{E}+2 \\ & 9 \end{aligned}$ | $1.32781 \mathrm{E}+17$ | 1.60851E+16 | $6.59031 \mathrm{E}+16$ |
| 47 | near star | $\begin{array}{\|l} \hline 1.19298 \mathrm{E}+3 \\ 0 \\ \hline \end{array}$ | $4.78813 \mathrm{E}+16$ | $9.19484 \mathrm{E}+16$ | $1.08903 \mathrm{E}+17$ |
| 48 | near star | $\begin{array}{\|l} \hline 1.65028 \mathrm{E}+3 \\ 0 \\ \hline \end{array}$ | 1.04974E+16 | $1.34655 \mathrm{E}+17$ | $7.02332 \mathrm{E}+16$ |
| 49 | near star | $\begin{aligned} & \hline 8.94731 \mathrm{E}+2 \\ & 9 \end{aligned}$ | $4.59519 \mathrm{E}+16$ | $8.94752 \mathrm{E}+15$ | 1.44982E+17 |
| 50 | near star | $\begin{aligned} & 5.96488 \mathrm{E}+2 \\ & 9 \end{aligned}$ | $1.36804 \mathrm{E}+17$ | $5.36738 \mathrm{E}+16$ | $5.10992 \mathrm{E}+16$ |
| 51 | near star | $\begin{aligned} & 2.00817 \mathrm{E}+3 \\ & 0 \end{aligned}$ | 1.77107E+16 | 2.7082E+16 | $1.52249 \mathrm{E}+17$ |
| 52 | near star | $\begin{aligned} & \hline 8.94731 \mathrm{E}+2 \\ & 9 \end{aligned}$ | $-1.0952 \mathrm{E}+17$ | $9.68318 \mathrm{E}+16$ | 5.3829E+16 |
| 53 | near star | $\begin{aligned} & 1.88888 \mathrm{E}+3 \\ & 0 \end{aligned}$ | $4.72306 \mathrm{E}+16$ | $1.16764 \mathrm{E}+17$ | $9.36129 E+16$ |
| 54 | near star | $\begin{array}{\|l\|} \hline 5.09003 E+3 \\ 0 \end{array}$ | $9.79121 \mathrm{E}+16$ | $-9.2465 E+16$ | $8.39443 E+16$ |
| 55 | near star | $\begin{aligned} & 3.97658 \mathrm{E}+2 \\ & 9 \end{aligned}$ | 1.09829E+17 | $9.70466 \mathrm{E}+16$ | $6.62157 \mathrm{E}+16$ |
| 56 | near star | $\begin{array}{\|l\|} \hline 7.95317 \mathrm{E}+2 \\ 9 \\ \hline \end{array}$ | $9.10748 \mathrm{E}+16$ | $1.36971 \mathrm{E}+17$ | $2.48893 \mathrm{E}+16$ |
| 57 | near star | $\begin{array}{\|l\|} \hline 1.09356 \mathrm{E}+3 \\ 0 \\ \hline \end{array}$ | -7.0043E+16 | 9.14497E+16 | 1.2171E+17 |
| 58 | near star | $\begin{aligned} & \hline 5.96488 \mathrm{E}+2 \\ & 9 \end{aligned}$ | $2.64948 \mathrm{E}+16$ | $4.32255 \mathrm{E}+16$ | 1.61635E+17 |
| 59 | near star | $\begin{array}{\|l} \hline 1.49122 \mathrm{E}+3 \\ 0 \\ \hline \end{array}$ | $3.16721 \mathrm{E}+16$ | $1.25283 E+17$ | 1.1067E+17 |
| 60 | near star | $\begin{array}{\|l} \hline 7.95317 \mathrm{E}+2 \\ 9 \end{array}$ | 4.73982E+16 | $1.59067 \mathrm{E}+15$ | 1.63433E+17 |
| 61 | near star | $\begin{aligned} & \hline 5.96488 \mathrm{E}+2 \\ & 9 \end{aligned}$ | 1.20195E+17 | $-9.0224 \mathrm{E}+16$ | $8.74395 \mathrm{E}+16$ |
| 62 | near star | $\begin{aligned} & 8.94731 \mathrm{E}+2 \\ & 9 \end{aligned}$ | $5.75703 \mathrm{E}+16$ | $-1.4009 \mathrm{E}+17$ | $8.88539 \mathrm{E}+16$ |


| 63 | near star | $\begin{aligned} & 7.95317 \mathrm{E}+2 \\ & 9 \end{aligned}$ | $6.76572 \mathrm{E}+16$ | $4.60048 \mathrm{E}+16$ | $1.57068 \mathrm{E}+17$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 64 | near star | $\begin{aligned} & 2.12747 E+3 \\ & 0 \end{aligned}$ | -9.2162E+16 | $1.20447 \mathrm{E}+17$ | 9.30606E+16 |
| 65 | near star | $\begin{aligned} & 8.94731 \mathrm{E}+2 \\ & 9 \end{aligned}$ | $5.72296 \mathrm{E}+15$ | 1.76608E+17 | $2.27853 \mathrm{E}+16$ |
| 66 | near star | $\begin{aligned} & 5.96488 \mathrm{E}+2 \\ & 9 \end{aligned}$ | $1.34996 \mathrm{E}+17$ | $1.16182 \mathrm{E}+17$ | $1.30636 \mathrm{E}+16$ |
| 67 | near star | $\begin{array}{\|l} \hline 5.96488 \mathrm{E}+2 \\ 9 \\ \hline \end{array}$ | $1.19512 \mathrm{E}+17$ | $4.88067 \mathrm{E}+16$ | -1.2445E+17 |
| 68 | near star | $\begin{array}{\|l\|} \hline 9.94146 \mathrm{E}+2 \\ 9 \\ \hline \end{array}$ | 7.87302E+16 | $1.638 \mathrm{E}+16$ | $1.62411 \mathrm{E}+17$ |
| 69 | near star | $\begin{array}{\|l\|} \hline 1.82923 E+3 \\ 0 \\ \hline \end{array}$ | 3.91777E+16 | 1.47326E+17 | $9.98492 \mathrm{E}+16$ |
| 70 | near star | $\begin{aligned} & 6.95902 \mathrm{E}+2 \\ & 9 \end{aligned}$ | 1.67294E+17 | $1.18466 \mathrm{E}+16$ | $7.32836 \mathrm{E}+16$ |
| 71 | near star | $\begin{aligned} & 8.94731 E+2 \\ & 9 \end{aligned}$ | $1.39077 \mathrm{E}+17$ | $9.10857 \mathrm{E}+16$ | 7.67253E+16 |
| 72 | near star | $\begin{aligned} & 2.78361 \mathrm{E}+3 \\ & 0 \\ & \hline \end{aligned}$ | $5.24234 \mathrm{E}+16$ | $1.59364 \mathrm{E}+16$ | $1.75315 \mathrm{E}+17$ |
| 73 | near star | $\begin{aligned} & 1.65028 \mathrm{E}+3 \\ & 0 \end{aligned}$ | $3.6434 \mathrm{E}+15$ | $2.91335 \mathrm{E}+16$ | $1.81794 \mathrm{E}+17$ |
| 74 | near star | $\begin{aligned} & 9.94146 \mathrm{E}+2 \\ & 9 \end{aligned}$ | $9.07771 \mathrm{E}+16$ | 1.01639E+17 | 1.23937E+17 |
| 75 | near star | $\begin{aligned} & 1.88888 \mathrm{E}+3 \\ & 0 \end{aligned}$ | $6.41076 \mathrm{E}+15$ | 1.79687E+16 | $1.83691 \mathrm{E}+17$ |
| 76 | near star | $\begin{array}{\|l} \hline 1.88888 \mathrm{E}+3 \\ 0 \\ \hline \end{array}$ | $2.06314 \mathrm{E}+15$ | $5.39393 \mathrm{E}+15$ | 1.86646E+17 |
| 77 | near star | $\begin{aligned} & 2.18712 \mathrm{E}+3 \\ & 0 \end{aligned}$ | 1.0974E+17 | $3.31921 \mathrm{E}+16$ | $1.4771 \mathrm{E}+17$ |
| 78 | near star | $\begin{aligned} & 2.18712 \mathrm{E}+3 \\ & 0 \end{aligned}$ | $1.54154 \mathrm{E}+17$ | $1.01333 \mathrm{E}+17$ | $3.85252 \mathrm{E}+16$ |
| 79 | near star | $\begin{aligned} & \hline 5.96488 \mathrm{E}+2 \\ & 9 \end{aligned}$ | $4.30221 \mathrm{E}+16$ | $1.83542 \mathrm{E}+17$ | $8.55871 \mathrm{E}+15$ |
| 80 | near star | $\begin{aligned} & \hline 9.94146 \mathrm{E}+2 \\ & 9 \end{aligned}$ | 1.30645E+17 | 6.84493E+16 | $1.20949 \mathrm{E}+17$ |
| 81 | near star | $\begin{array}{\|l\|} \hline 1.09356 \mathrm{E}+3 \\ 0 \\ \hline \end{array}$ | $1.31276 \mathrm{E}+17$ | $6.75268 \mathrm{E}+16$ | $1.20784 \mathrm{E}+17$ |
| 82 | near star | $\begin{aligned} & 1.19298 \mathrm{E}+3 \\ & 0 \end{aligned}$ | $1.33898 \mathrm{E}+17$ | $5.20951 \mathrm{E}+16$ | 1.2578E+17 |
| 83 | near star | $\begin{array}{\|l\|} \hline 1.09356 \mathrm{E}+3 \\ 0 \\ \hline \end{array}$ | $2.19059 \mathrm{E}+16$ | 6.93128E+16 | $1.77114 \mathrm{E}+17$ |
| 84 | near star | $\begin{aligned} & 1.49122 \mathrm{E}+3 \\ & 0 \\ & \hline \end{aligned}$ | 3.99999E+16 | 8.00904E+16 | 1.70731E+17 |
| 85 | near star | $\begin{aligned} & 6.95902 \mathrm{E}+2 \\ & 9 \\ & \hline \end{aligned}$ | $2.19758 \mathrm{E}+16$ | $1.28321 \mathrm{E}+16$ | $-1.9175 \mathrm{E}+17$ |


| 86 | near star | $\begin{aligned} & 1.09356 \mathrm{E}+3 \\ & 0 \end{aligned}$ | $-1.3524 \mathrm{E}+17$ | $5.38681 \mathrm{E}+16$ | 1.27447E+17 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 87 | near star | $\begin{aligned} & 8.94731 \mathrm{E}+2 \\ & 9 \end{aligned}$ | $2.07383 \mathrm{E}+16$ | $9.28974 \mathrm{E}+15$ | $1.93754 \mathrm{E}+17$ |
| 88 | near star | $\begin{aligned} & 5.96488 \mathrm{E}+2 \\ & 9 \end{aligned}$ | $1.01434 \mathrm{E}+17$ | $8.45481 \mathrm{E}+16$ | $1.45159 \mathrm{E}+17$ |
| 89 | near star | $\begin{aligned} & 5.96488 \mathrm{E}+2 \\ & 9 \end{aligned}$ | $7.37726 \mathrm{E}+16$ | $5.17702 \mathrm{E}+16$ | $1.79009 \mathrm{E}+17$ |
| 90 | near star | $\begin{aligned} & 1.82923 \mathrm{E}+3 \\ & 0 \end{aligned}$ | $1.50711 \mathrm{E}+17$ | $6.46728 \mathrm{E}+16$ | $1.16827 \mathrm{E}+17$ |
| 91 | near star | $\begin{aligned} & \hline 6.95902 \mathrm{E}+2 \\ & 9 \\ & \hline \end{aligned}$ | $3.30768 \mathrm{E}+16$ | $1.22256 \mathrm{E}+17$ | $1.58766 \mathrm{E}+17$ |
| 92 | Glob Clus Group | $\begin{aligned} & 1.20578 \mathrm{E}+3 \\ & 7 \end{aligned}$ | $1.16925 \mathrm{E}+21$ | $1.04245 \mathrm{E}+21$ | $9.31497 \mathrm{E}+19$ |
| 93 | Glob Clus Group | $\begin{aligned} & 7.43305 \mathrm{E}+3 \\ & 6 \end{aligned}$ | $1.79414 \mathrm{E}+20$ | $3.61781 \mathrm{E}+20$ | $1.42253 \mathrm{E}+19$ |
| 94 | Glob Clus Group | $\begin{aligned} & 9.58802 \mathrm{E}+3 \\ & 6 \end{aligned}$ | 1.48744E+19 | $2.77665 \mathrm{E}+19$ | $7.91706 \mathrm{E}+19$ |
| 95 | Glob Clus Group | $\begin{aligned} & 7.05555 \mathrm{E}+3 \\ & 6 \\ & \hline \end{aligned}$ | $6.94375 \mathrm{E}+19$ | $4.44352 \mathrm{E}+18$ | 7.944E+17 |
| 96 | Glob Clus Group | $\begin{aligned} & 6.46631 \mathrm{E}+3 \\ & 6 \end{aligned}$ | $9.11252 \mathrm{E}+19$ | $4.39257 \mathrm{E}+19$ | $1.89032 \mathrm{E}+20$ |
| 97 | Glob Clus Group | $\begin{aligned} & 7.23385 \mathrm{E}+3 \\ & 6 \end{aligned}$ | $1.05314 \mathrm{E}+20$ | $2.06504 \mathrm{E}+19$ | $8.97721 \mathrm{E}+19$ |
| 98 | Glob Clus Group | $\begin{aligned} & \text { 6.79923E+3 } \\ & 6 \end{aligned}$ | 1.25702E+20 | $6.15542 \mathrm{E}+19$ | $3.76993 \mathrm{E}+19$ |
| 99 | Glob Clus Group | $\begin{aligned} & 8.07244 \mathrm{E}+3 \\ & 6 \end{aligned}$ | $1.5288 \mathrm{E}+20$ | $2.40773 \mathrm{E}+19$ | $1.58338 \mathrm{E}+19$ |
| 100 | Glob Clus Group | $\begin{aligned} & 9.57827 \mathrm{E}+3 \\ & 6 \end{aligned}$ | $1.74887 \mathrm{E}+20$ | $1.35743 \mathrm{E}+19$ | $3.13919 \mathrm{E}+19$ |
| 101 | Glob Clus Group | $8.2981 \mathrm{E}+36$ | $1.85602 \mathrm{E}+20$ | $5.87126 \mathrm{E}+19$ | $1.50955 \mathrm{E}+19$ |
| 102 | Glob Clus Group | $\begin{aligned} & 1.03904 \mathrm{E}+3 \\ & 7 \end{aligned}$ | $2.00762 \mathrm{E}+20$ | $1.02368 \mathrm{E}+20$ | 7.89348E+19 |
| 103 | Glob Clus Group | $\begin{aligned} & 8.99599 E+3 \\ & 6 \end{aligned}$ | $2.21232 \mathrm{E}+20$ | $1.03194 \mathrm{E}+19$ | $1.15685 \mathrm{E}+20$ |
| 104 | Glob Clus Group | $8.5572 \mathrm{E}+36$ | $2.40926 \mathrm{E}+20$ | $2.38732 \mathrm{E}+19$ | $8.08095 \mathrm{E}+18$ |
| 105 | Glob Clus Group | $\begin{aligned} & 9.81786 \mathrm{E}+3 \\ & 6 \\ & \hline \end{aligned}$ | $2.52521 \mathrm{E}+20$ | $1.04214 \mathrm{E}+19$ | $1.90968 \mathrm{E}+18$ |
| 106 | Glob Clus Group | $\begin{aligned} & 9.86105 \mathrm{E}+3 \\ & 6 \end{aligned}$ | $2.63724 \mathrm{E}+20$ | $1.58631 \mathrm{E}+19$ | $2.36248 \mathrm{E}+19$ |
| 107 | Glob Clus Group | $\begin{aligned} & 8.93192 \mathrm{E}+3 \\ & 6 \\ & \hline \end{aligned}$ | $2.80244 \mathrm{E}+20$ | 4.57404E+18 | $5.62166 \mathrm{E}+18$ |
| 108 | Glob Clus Group | $\begin{aligned} & 1.00965 \mathrm{E}+3 \\ & 7 \end{aligned}$ | $2.93615 \mathrm{E}+20$ | $2.52379 \mathrm{E}+19$ | $6.36066 \mathrm{E}+18$ |
| 109 | Glob Clus Group | $1.37127 \mathrm{E}+3$ | $3.13834 \mathrm{E}+20$ | - | $1.46617 \mathrm{E}+19$ |

$\left.\begin{array}{|l|l|l|l|l|l|}\hline & & 7 & & 1.18077 \mathrm{E}+18 & \\ \hline 110 & \text { Glob Clus Group } & \begin{array}{l}1.01466 \mathrm{E}+3 \\ 7\end{array} & 3.35306 \mathrm{E}+20 & - \\ 1.68075 \mathrm{E}+20 & -3.47826 \mathrm{E}+19 \\ \hline 111 & \text { Glob Clus Group } & \begin{array}{l}1.11914 \mathrm{E}+3 \\ 7\end{array} & 3.72364 \mathrm{E}+20 & 1.37362 \mathrm{E}+19 & - \\ \hline 112 & \text { Glob Clus Group } & 1.02218 \mathrm{E}+3 \\ 7\end{array}\right)$

| 133 | Triangulum <br> Galaxy | $1.41 \mathrm{E}+41$ | $1.28546 \mathrm{E}+20$ | $1.93083 \mathrm{E}+22$ | $-1.82029 \mathrm{E}+22$ |
| :--- | :--- | :--- | :--- | :--- | :--- |

Table 1: Giving the initial values of all the point masses, their respective masses in Kg , and their x z Cartesian positions.

| $\begin{aligned} & \text { Exp } \\ & \text { t SI. } \\ & \text { No } \end{aligned}$ | Ti <br> me <br> ste <br> p | No of itera tion s | File name | Initial position ofneutrino |  |  | Final position of neutrino |  |  | GenR el Deflec tion degre es / 10000 0 | Calculat ed Solar elongati on angle in degrees | SITA <br> Deflecti on degree s / 100000 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | S X | sy | SZ | S X | sy | Sz |  |  |  |
| 1 | 0.1 | 40 | Vvtc vy -c. x Ro. $40 \times 0.1 \mathrm{~s}$ <br> 4.6552.x/s | $\begin{aligned} & 6959 \\ & 9999 \\ & 8.6 \\ & \hline \end{aligned}$ | $\begin{array}{\|l\|l} 29979 \\ 245.8 \end{array}$ | $\begin{aligned} & 1.344 \\ & 2 \mathrm{E}-11 \end{aligned}$ | $\begin{aligned} & 695998 \\ & 564 \end{aligned}$ | $\begin{aligned} & 1169190 \\ & 027 \end{aligned}$ | $\begin{aligned} & -2.04 \mathrm{E}- \\ & 08 \end{aligned}$ | $\begin{aligned} & 0.1168 \\ & 8 \end{aligned}$ | $\begin{aligned} & 11.5952 \\ & 7069 \end{aligned}$ | $\begin{aligned} & 10.446 \\ & 4361 \end{aligned}$ |
| 2 | 0.1 | 40 | Vvtc vy eq c.x eq 2c 40x.1s result 6.714.xls | $\begin{aligned} & 5995 \\ & 8491 \\ & 5.5 \\ & \hline \end{aligned}$ | $\begin{array}{\|l\|l} 29979 \\ 245.8 \end{array}$ | $\begin{array}{\|l} \hline 6959 \\ 9999 \\ 9 \\ \hline \end{array}$ | $\begin{aligned} & 599584 \\ & 312 \end{aligned}$ | $\begin{aligned} & 1169190 \\ & 284 \\ & \hline \end{aligned}$ | $\begin{aligned} & 695999 \\ & 299 \end{aligned}$ | $\begin{aligned} & 3.99 E \\ & +15 \end{aligned}$ | $\begin{aligned} & 11.5952 \\ & 7069 \end{aligned}$ | $\begin{aligned} & 7.2424 \\ & 9697 \end{aligned}$ |
| 3 | 0.1 | 40 | Vvtc $40 \times 0.1 \mathrm{~s}$ Y 1.2 Radi result 3.48905.xls | $\begin{aligned} & 126.4 \\ & 1240 \\ & 44 \end{aligned}$ | $\begin{aligned} & 2.7723 \\ & \mathrm{E}-07 \end{aligned}$ | $\begin{aligned} & 8351 \\ & 9972 \\ & 8 \end{aligned}$ | $\begin{aligned} & 569605 \\ & 932 \end{aligned}$ | $\begin{array}{\|l} - \\ \hline 1.05415 \\ \mathrm{E}-06 \end{array}$ | $\begin{aligned} & 835198 \\ & 835 \end{aligned}$ | $\begin{aligned} & 4.79 E \\ & +15 \end{aligned}$ | $\begin{aligned} & 11.5952 \\ & 7069 \end{aligned}$ | $\begin{aligned} & 11.615 \\ & 0876 \end{aligned}$ |
| 4 | 0.1 | 40 | Vvtc $40 \times 0.1 \mathrm{~s}$ Y 1.5 Radi result 4.094753.xls | $\begin{aligned} & 2997 \\ & 9325 . \\ & 19 \\ & \hline \end{aligned}$ | $\begin{aligned} & 3.0566 \\ & \mathrm{E}-07 \end{aligned}$ | $\begin{aligned} & 1043 \\ & 9997 \\ & 85 \end{aligned}$ | $\begin{aligned} & 569605 \\ & 822 \end{aligned}$ | $\begin{array}{\|l\|} \hline- \\ 1.05419 \\ E-06 \end{array}$ | $\begin{aligned} & 104399 \\ & 9202 \end{aligned}$ | $\begin{array}{\|l} 5.98 \mathrm{E} \\ +15 \end{array}$ | $\begin{array}{\|l\|l} 11.5952 \\ 7069 \end{array}$ | $\begin{aligned} & 7.9175 \\ & 7108 \end{aligned}$ |
| 5 | 0.1 | 40 | Vvtc $40 \times 0.1 \mathrm{~s}$ Y 2 Radi result 5.167069.xls | $\begin{array}{\|l} 34.66 \\ 4776 \\ 83 \\ \hline \end{array}$ | $\begin{aligned} & 2.7726 \\ & \mathrm{E}-07 \end{aligned}$ | $\begin{aligned} & 1391 \\ & 9998 \\ & 81 \end{aligned}$ | $\begin{aligned} & 569605 \\ & 742 \end{aligned}$ | $\begin{array}{\|l\|} \hline- \\ 1.05426 \\ E-06 \end{array}$ | $\begin{aligned} & 139199 \\ & 9524 \end{aligned}$ | $\begin{aligned} & 7.98 \mathrm{E} \\ & +15 \end{aligned}$ | $\begin{aligned} & 11.5952 \\ & 7069 \end{aligned}$ | $\begin{aligned} & 4.7058 \\ & 3429 \end{aligned}$ |
| 6 | 0.1 | 40 | Vvtc 40x0.1s Y 3 Radi result 7.424343.xls | $\begin{array}{\|l} 11.20 \\ 7476 \\ 24 \end{array}$ | $2.773 \mathrm{E}$ -07 | $\begin{aligned} & 2087 \\ & 9999 \\ & 43 \end{aligned}$ | $\begin{aligned} & 569605 \\ & 693 \end{aligned}$ | $\begin{array}{\|l} 1.05442 \\ \mathrm{E}-06 \end{array}$ | $\begin{aligned} & 208799 \\ & 9778 \end{aligned}$ | $\begin{aligned} & 1.2 \mathrm{E}+ \\ & 16 \end{aligned}$ | $\begin{aligned} & 11.5952 \\ & 7069 \end{aligned}$ | $\begin{array}{\|l} 2.1833 \\ 9152 \end{array}$ |
| 7 | 0.1 | 40 | Vvtc $40 \times 0.1 \mathrm{~s}$ Y 10 Radi result 23.25372.xls | $\begin{aligned} & 0.324 \\ & 0519 \\ & 2 \\ & \hline \end{aligned}$ | $\begin{aligned} & 2.7782 \\ & \mathrm{E}-07 \end{aligned}$ | $\begin{aligned} & 6959 \\ & 9999 \\ & 95 \end{aligned}$ | $\begin{aligned} & 569605 \\ & 671 \end{aligned}$ | $\begin{aligned} & - \\ & 1.05639 \\ & E-06 \end{aligned}$ | $\begin{aligned} & 695999 \\ & 9979 \end{aligned}$ | $\begin{array}{\|l} 3.99 E \\ +16 \end{array}$ | $\begin{aligned} & 11.5952 \\ & 7069 \end{aligned}$ | $\begin{array}{\|l} 0.2091 \\ 3098 \end{array}$ |
| 8 | 0.1 | 40 | vak variable time create vak1 40x 0.1 NORMAL radius | $\begin{aligned} & 6959 \\ & 9965 \\ & 0.8 \end{aligned}$ | $190.33$ $1964$ | $\begin{aligned} & 5.390 \\ & 2 \mathrm{E}-09 \end{aligned}$ | $\begin{aligned} & 695998 \\ & 440 \end{aligned}$ | $\begin{aligned} & 5696060 \\ & 64.7 \end{aligned}$ | $\begin{aligned} & 2.0473 \\ & \text { E-08 } \end{aligned}$ | $0.1173$ | $\begin{array}{\|l\|l} 11.5952 \\ 7069 \end{array}$ | $\begin{aligned} & 15.632 \\ & 2201 \end{aligned}$ |


|  |  |  | $\begin{array}{\|l\|} \hline \text { result } \\ 3.11093 . x l s \end{array}$ |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 9 | 0.1 | 40 | vak variable time create vak1 40x $0.1 \mathrm{~s} \quad 3$ radius result 7.24.xls | $\begin{aligned} & 2087 \\ & 9999 \\ & 43 \end{aligned}$ | 11.207 <br> 4768 | $\begin{aligned} & 5.556 \\ & 7 \mathrm{E}-09 \end{aligned}$ | $\begin{aligned} & 208799 \\ & 9778 \end{aligned}$ | $\begin{aligned} & 5696056 \\ & 93.3 \end{aligned}$ | $\begin{array}{\|l} 2.1104 \\ \mathrm{E}-08 \end{array}$ | $\begin{aligned} & 0.1209 \\ & 2 \end{aligned}$ | $\begin{aligned} & 11.5952 \\ & 7069 \end{aligned}$ | $\begin{aligned} & 2.1833 \\ & 9152 \end{aligned}$ |
| 10 | 0.1 | 160 | Vvtc vx 0.25c.vy 0.97c, x $2 e 8$ y $6 e 8$ z 5e11 $160 \times 0.1$ s result 0.797441 extr Good | $\begin{aligned} & 5761 \\ & 9336 . \\ & 65 \end{aligned}$ | $\begin{aligned} & 13320 \\ & 063.2 \end{aligned}$ | $\begin{aligned} & 4.971 \\ & 4 \mathrm{E}+1 \\ & 1 \end{aligned}$ | $\begin{aligned} & - \\ & 871737 \\ & 283 \end{aligned}$ | $\begin{aligned} & 3586062 \\ & 665 \end{aligned}$ | $\begin{aligned} & 4.9714 \\ & E+11 \end{aligned}$ | $\begin{array}{\|l} \hline 2.85 \mathrm{E} \\ +18 \end{array}$ | $\begin{aligned} & 26.0727 \\ & 8278 \end{aligned}$ | $\begin{aligned} & 0.0853 \\ & 7736 \end{aligned}$ |
| 11 | 0.1 | 80 | Vvtc vx vz 0.25c.vy 0.93c, y Ro. 80x0.1s result 0.7345 V GOOD IMP.xls | $\begin{aligned} & 1798 \\ & 7495 \\ & 5 \end{aligned}$ | $\begin{aligned} & 22967 \\ & 354.8 \end{aligned}$ | $\begin{array}{\|l} - \\ 1798 \\ 7495 \\ 5 \end{array}$ | 592077 652 | $\begin{array}{\|l} 1519405 \\ 093 \end{array}$ | $592077$ $652$ | $\begin{aligned} & 3.4 \mathrm{E}+ \\ & 15 \end{aligned}$ | $\begin{array}{\|l\|l} \hline 29.9948 \\ 7522 \end{array}$ | $\begin{aligned} & 66.203 \\ & 7468 \end{aligned}$ |
| 12 | 0.1 | 40 | Vvtc -vy vz eq .7c.x eq 2c 40x result 12.032.1s.xls | $\begin{array}{\|l} 5995 \\ 8491 \\ 5.5 \end{array}$ | $\begin{aligned} & 21198 \\ & 528 \end{aligned}$ | $\begin{aligned} & 7171 \\ & 9852 \\ & 7 \end{aligned}$ | $\begin{aligned} & 599584 \\ & 480 \end{aligned}$ | $\begin{array}{\|l} \hline 8267424 \\ 60.5 \end{array}$ | $\begin{aligned} & 152274 \\ & 1954 \end{aligned}$ | $\begin{array}{\|l} 8.72 \mathrm{E} \\ +15 \end{array}$ | $\begin{aligned} & 46.1565 \\ & 8888 \end{aligned}$ | $\begin{aligned} & 4.0416 \\ & 9627 \end{aligned}$ |
| 13 | 0.1 | 160 | Vvtc vy vz 0.7c. $x$ Ro. 80x0.1s result 4.169102.xls | $\begin{aligned} & 6960 \\ & 0249 \\ & 8.6 \end{aligned}$ | $\begin{aligned} & 21198 \\ & 528 \end{aligned}$ | $\begin{aligned} & 2119 \\ & 8528 \end{aligned}$ | $\begin{aligned} & 695998 \\ & 662 \end{aligned}$ | $\begin{aligned} & 1674682 \\ & 200 \end{aligned}$ | $167468$ $2200$ | $\begin{aligned} & 9.6 \mathrm{E}+ \\ & 15 \end{aligned}$ | $\begin{array}{\|l} 46.1587 \\ 618 \end{array}$ | $\begin{aligned} & 11.664 \\ & 5604 \end{aligned}$ |
| 14 | 0.1 | 160 | Vvtc vz vy 0.7c. x Ro yz 2.8e08 $264 \times 0.1 \mathrm{~s}$ result 2.0309 <br> GOOD.xls | $\begin{aligned} & 6960 \\ & 1216 \\ & 0.8 \end{aligned}$ | $\begin{aligned} & 64349 \\ & 34.11 \end{aligned}$ | $\begin{aligned} & 6434 \\ & 934.1 \\ & 1 \end{aligned}$ | $\begin{aligned} & 695998 \\ & 984 \end{aligned}$ | $\begin{array}{\|l} 2770573 \\ 788 \end{array}$ | $\begin{aligned} & 277057 \\ & 3788 \end{aligned}$ | $\begin{aligned} & 1.6 \mathrm{E}+ \\ & 16 \end{aligned}$ | $\begin{array}{\|l} \hline 46.1587 \\ 724 \end{array}$ | $\begin{aligned} & 23.944 \\ & 8121 \end{aligned}$ |
| 15 | 0.1 | 160 | Vvtc vz vy 0.7c. <br> $x$ Ro. $160 \times 0.1 \mathrm{~s}$ result 2.083574 <br> v Good.xls | $\begin{array}{\|l} 6960 \\ 0536 \\ 3.3 \end{array}$ | $\begin{aligned} & 9.0590 \\ & 489 \end{aligned}$ | $\begin{array}{\|l} 9.059 \\ 0567 \\ 3 \end{array}$ | $\begin{aligned} & 695996 \\ & 805 \end{aligned}$ | $\begin{aligned} & 1674682 \\ & 214 \end{aligned}$ | $167468$ $2214$ | $\begin{array}{\|l} 9.6 \mathrm{E}+ \\ 15 \end{array}$ | $\begin{array}{\|l} 46.1587 \\ 804 \end{array}$ | $\begin{aligned} & 23.340 \\ & 0541 \end{aligned}$ |


| 16 | 0.1 | 160 | Vvtc vz vy 0.7c. $x$ Ro yz 8e08 160x0.1s result 2.181198 Good.xls | $\begin{aligned} & 6959 \\ & 9930 \\ & 2.4 \end{aligned}$ | $\begin{array}{\|l\|} 55432 \\ 72.01 \end{array}$ | $\begin{array}{\|l} 5543 \\ 272.0 \\ 1 \end{array}$ | $\begin{aligned} & 695986 \\ & 377 \end{aligned}$ | $\begin{aligned} & 2570560 \\ & 903 \end{aligned}$ | $257056$ $0903$ | $\begin{aligned} & 1.5 \mathrm{E}+ \\ & 16 \end{aligned}$ | $\begin{array}{\|l} 46.1587 \\ 804 \end{array}$ | $\begin{aligned} & 22.295 \\ & 4287 \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 17 | 0.1 | 160 | Vvtc vz vy 0.7c. $x$ Ro yz 4e08 160x0.1s result 2.473451 Good.xls | $\begin{aligned} & 6959 \\ & 9967 \\ & 1.9 \end{aligned}$ | 27715 <br> 39.85 | $\begin{array}{\|l} 2771 \\ 539.8 \\ 5 \end{array}$ | $\begin{aligned} & 695986 \\ & 439 \end{aligned}$ | $\begin{aligned} & 2970558 \\ & 735 \end{aligned}$ | $\begin{array}{\|l\|} \hline- \\ 297055 \\ 8735 \end{array}$ | $\begin{aligned} & 1.7 \mathrm{E}+ \\ & 16 \end{aligned}$ | $\begin{array}{\|l} 46.1587 \\ 804 \end{array}$ | $\begin{array}{\|l\|} 19.661 \\ 0928 \end{array}$ |
| 18 | 0.1 | 160 | Vvtc vz vy 0.7c. $x$ Ro yz 6e08 160x0.1s result 2.27 Good.xIs | $\begin{array}{\|l} 6959 \\ 9948 \end{array}$ $8.7$ | $\begin{aligned} & 64418 \\ & 56.72 \end{aligned}$ | $\begin{aligned} & 6441 \\ & 856.7 \\ & 2 \end{aligned}$ | $\begin{aligned} & 695986 \\ & 065 \end{aligned}$ | $\begin{array}{\|l} \hline 2770559 \\ 962 \end{array}$ | 277055 9962 | $\begin{aligned} & 1.6 \mathrm{E}+ \\ & 16 \end{aligned}$ | $\begin{array}{\|l} 46.1587 \\ 804 \end{array}$ | $\begin{aligned} & 21.369 \\ & 7685 \end{aligned}$ |
| 19 | 0.1 | 160 | Vvtc vz vy 0.7c. $x$ Ro yz 6e08 $160 \times 0.1 \mathrm{~s}$ result 2.2456 Good.xls | $\begin{aligned} & 6959 \\ & 9941 \\ & 3.6 \end{aligned}$ | $\begin{aligned} & 71536 \\ & 81.74 \end{aligned}$ | $\begin{aligned} & 7153 \\ & 681.7 \\ & 4 \\ & \hline \end{aligned}$ | $\begin{aligned} & 695986 \\ & 096 \end{aligned}$ | $\begin{array}{\|l} 2720560 \\ 223 \end{array}$ | $272056$ $0223$ | $\begin{aligned} & 1.6 \mathrm{E}+ \\ & 16 \end{aligned}$ | $\begin{array}{\|l} 46.1587 \\ 804 \end{array}$ | $\begin{aligned} & 21.655 \\ & 746 \end{aligned}$ |
| 20 | 0.1 | 160 | Vvtc vz vy 0.7c. x Ro yz 6.2e08 $160 \times 0.1 \mathrm{~s}$ result 2.605 Good.xls | $\begin{aligned} & 6959 \\ & 9946 \\ & 8.4 \end{aligned}$ | $\begin{array}{\|l} 52433 \\ 44.22 \end{array}$ | $\begin{aligned} & 5243 \\ & 344.2 \\ & 2 \end{aligned}$ | $\begin{aligned} & 695986 \\ & 073 \end{aligned}$ | $\begin{array}{\|l} 2750560 \\ 069 \end{array}$ | $275056$ $0069$ | $\begin{aligned} & 1.6 \mathrm{E}+ \\ & 16 \end{aligned}$ | $\begin{array}{\|l} 46.1587 \\ 804 \end{array}$ | $\begin{aligned} & 21.489 \\ & 3317 \end{aligned}$ |
| 21 | 0.1 | 160 | Vvtc vz vy 0.7c. x Ro yz 5.8e08 $160 \times 0.1$ s result 2.89314 Good.xls | $\begin{aligned} & 6959 \\ & 9950 \\ & 9.5 \end{aligned}$ | $\begin{aligned} & 76403 \\ & 69.05 \end{aligned}$ | $\begin{aligned} & 7640 \\ & 369.0 \\ & 5 \end{aligned}$ | $\begin{aligned} & 695986 \\ & 064 \end{aligned}$ | $\begin{aligned} & - \\ & 2790559 \\ & 852 \end{aligned}$ | $279055$ | $\begin{aligned} & 1.6 \mathrm{E}+ \\ & 16 \end{aligned}$ | $\begin{array}{\|l} 46.1587 \\ 804 \end{array}$ | $\begin{aligned} & 21.242 \\ & 4991 \end{aligned}$ |
| 22 | 0.1 | 160 | Vvtc vz vy 0.7c. x Ro yz 5.5e08 $160 \times 0.1 \mathrm{~s}$ result 2.311574 Good.xls | $\begin{aligned} & 6959 \\ & 9951 \\ & 8.4 \end{aligned}$ | $\begin{array}{\|l\|l\|} 11611 \\ 18.37 \end{array}$ | $\begin{array}{\|l} - \\ -1161 \\ 118.3 \\ 7 \end{array}$ | $\begin{aligned} & 695986 \\ & 077 \end{aligned}$ | $\begin{array}{\|l} 2820559 \\ 682 \end{array}$ | $282055$ $9682$ | $\begin{array}{\|l} 1.6 \mathrm{E}+ \\ 16 \end{array}$ | $\begin{array}{\|l} 46.1587 \\ 804 \end{array}$ | $\begin{array}{\|l} 21.036 \\ 2966 \end{array}$ |
| 23 | 0.1 | 160 | Vvtc vz vy 0.7c. $x$ Ro yz 4e08 160x0.1s result 2.220438 Good.xls | $\begin{aligned} & 6959 \\ & 9967 \\ & 1.9 \end{aligned}$ | 27715 <br> 39.85 | $\begin{array}{\|l\|} \hline- \\ 2771 \\ 539.8 \\ 5 \end{array}$ | $\begin{aligned} & 695986 \\ & 161 \end{aligned}$ | $\begin{array}{\|l} 2670560 \\ 467 \end{array}$ | $267056$ $0467$ | $\begin{aligned} & 1.5 \mathrm{E}+ \\ & 16 \end{aligned}$ | $\begin{array}{\|l} 46.1587 \\ 804 \end{array}$ | $\begin{aligned} & 21.901 \\ & 4159 \end{aligned}$ |


| 24 | 0.1 | 160 | Vvtc vz vy 0.7c. $x$ Ro yz 4e08 160x0.1s result 2.220438 Good1.xls | $\begin{aligned} & 6959 \\ & 9939 \\ & 0.8 \end{aligned}$ | $\begin{aligned} & 44929 \\ & 3.027 \end{aligned}$ | $\begin{aligned} & 4492 \\ & 93.02 \\ & 7 \end{aligned}$ | $\begin{aligned} & 695986 \\ & 161 \end{aligned}$ | $\begin{aligned} & -\quad 2670560 \\ & 467 \end{aligned}$ | $\begin{aligned} & 2.671 \mathrm{E} \\ & +09 \end{aligned}$ | $\begin{aligned} & 1.5 \mathrm{E}+ \\ & 16 \end{aligned}$ | $\begin{aligned} & 46.1587 \\ & 804 \end{aligned}$ | $\begin{aligned} & 21.901 \\ & 4159 \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 25 | 0.1 | 160 | Vvtc vz vy 0.7c. $x$ Ro yz 2e08 160x0.1s result 2.9314.xls | $\begin{aligned} & 6959 \\ & 9987 \\ & 9.2 \end{aligned}$ | $\begin{aligned} & 11984 \\ & 981.4 \end{aligned}$ | $\begin{aligned} & 1198 \\ & 4981 . \\ & 4 \end{aligned}$ | $\begin{aligned} & 695988 \\ & 030 \end{aligned}$ | $\begin{array}{\|l} 3170557 \\ 360 \end{array}$ | $\begin{aligned} & 317055 \\ & 7360 \end{aligned}$ | $\begin{aligned} & 1.8 \mathrm{E}+ \\ & 16 \end{aligned}$ | $\begin{aligned} & 46.1587 \\ & 804 \end{aligned}$ | $\begin{aligned} & 16.589 \\ & 3734 \end{aligned}$ |
| 26 | 0.1 | 160 | Vvtc vz vy 0.7c. $x$ Ro yz 1e09 160x0.1s result 2.1318 Good.xls | $\begin{aligned} & 6959 \\ & 9920 \\ & 7.5 \end{aligned}$ | $\begin{aligned} & 36701 \\ & 21.84 \end{aligned}$ | $\begin{aligned} & 3670 \\ & 121.8 \\ & 4 \end{aligned}$ | $\begin{aligned} & 695987 \\ & 045 \end{aligned}$ | $\begin{array}{\|l} 2370561 \\ 602 \end{array}$ | $237056$ $1602$ | $\begin{aligned} & 1.4 \mathrm{E}+ \\ & 16 \end{aligned}$ | $\begin{aligned} & 46.1587 \\ & 804 \end{aligned}$ | $\begin{aligned} & 22.812 \\ & 0586 \end{aligned}$ |
| 27 | 0.1 | 160 | Vvtc vz vy 0.7c. x Ro yz 1.4e09 160x0.1s result 2.090797.xls | $\begin{aligned} & 6959 \\ & 9904 \\ & 1.7 \end{aligned}$ | $\begin{aligned} & 89842 \\ & 6.816 \end{aligned}$ | $\begin{aligned} & 8984 \\ & 26.81 \\ & 6 \end{aligned}$ | $\begin{aligned} & 695988 \\ & 869 \end{aligned}$ | $\begin{aligned} & 1970562 \\ & 510 \end{aligned}$ | $\begin{aligned} & 197056 \\ & 2510 \end{aligned}$ | $\begin{aligned} & 1.1 \mathrm{E}+ \\ & 16 \end{aligned}$ | $\begin{aligned} & 46.1587 \\ & 804 \end{aligned}$ | $\begin{aligned} & 23.265 \\ & 2927 \end{aligned}$ |
| 28 | 0.1 | 160 | Vvtc vz vy 0.7c. x 3437 Ro. $160 \times 0.1 \mathrm{~s}$ result 2.104776.xls | $\begin{aligned} & 6960 \\ & 0262 \\ & 2.5 \end{aligned}$ | $\begin{aligned} & 83149 \\ & 93.67 \end{aligned}$ | $\begin{aligned} & 8314 \\ & 993.6 \\ & 7 \\ & \hline \end{aligned}$ | $\begin{aligned} & 695991 \\ & 441 \end{aligned}$ | $\begin{array}{\|l} 2170562 \\ 122 \end{array}$ | $\begin{aligned} & 217056 \\ & 2122 \end{aligned}$ | $\begin{aligned} & 1.2 \mathrm{E}+ \\ & 16 \end{aligned}$ | $\begin{aligned} & 46.1587 \\ & 804 \end{aligned}$ | $\begin{aligned} & 23.104 \\ & 9511 \end{aligned}$ |
| 29 | 0.1 | 160 | Vvtc vz vy 0.7c. x 0000 Ro. $160 \times 0.1 \mathrm{~s}$ result 2.104761 Good.xls | $\begin{array}{\|l} 6959 \\ 9908 \end{array}$ $5.5$ | $\begin{aligned} & 83149 \\ & 93.68 \end{aligned}$ | $\begin{aligned} & 8314 \\ & 993.6 \\ & 8 \end{aligned}$ | $\begin{aligned} & 695987 \\ & 904 \end{aligned}$ | $\begin{aligned} & 2170562 \\ & 122 \end{aligned}$ | $\begin{aligned} & 217056 \\ & 2122 \end{aligned}$ | $\begin{aligned} & 1.2 \mathrm{E}+ \\ & 16 \end{aligned}$ | $\begin{aligned} & 46.1587 \\ & 804 \end{aligned}$ | $\begin{array}{\|l} 23.105 \\ 1088 \end{array}$ |
| 30 | 0.1 | $\begin{aligned} & 200 \\ & 0 \end{aligned}$ | Vvtc vz 0.25c.vx 0.97c, yRo. x 2e8 z 6,5e8 2000x0.1s result 2.357395 Good.xls | $\begin{aligned} & 3511 \\ & 4073 . \\ & 22 \end{aligned}$ | $\begin{aligned} & 69599 \\ & 9620 \end{aligned}$ | $\begin{aligned} & 1234 \\ & 7120 . \\ & 7 \end{aligned}$ | $\begin{aligned} & 1.4782 \\ & E+10 \end{aligned}$ | $\begin{aligned} & 6957869 \\ & 80.5 \end{aligned}$ | $\begin{aligned} & 5.7375 \\ & \mathrm{E}+10 \end{aligned}$ | $\begin{aligned} & 3.3 \mathrm{E}+ \\ & 17 \end{aligned}$ | $\begin{aligned} & 46.1587 \\ & 804 \end{aligned}$ | $\begin{aligned} & 20.629 \\ & 1925 \end{aligned}$ |
| 31 | 0.1 | 160 | Vvtc vz 0.25c.vx 0.97c, yRo. x $2 e 8$ z 6,5e8 $160 \times 0.1$ s result 2.357032 Good.xls | $\begin{aligned} & 5012 \\ & 4424 . \\ & 53 \end{aligned}$ | $\begin{aligned} & 69599 \\ & 9562 \end{aligned}$ | $\begin{aligned} & 1570 \\ & 7474 . \\ & 8 \end{aligned}$ | $\begin{aligned} & 961675 \\ & 531 \end{aligned}$ | $\begin{array}{\|l} 6959862 \\ 15.7 \end{array}$ | $\begin{array}{\|l} 393438 \\ 7845 \end{array}$ | $\begin{aligned} & 2.3 \mathrm{E}+ \\ & 16 \end{aligned}$ | $\begin{aligned} & 46.1587 \\ & 804 \end{aligned}$ | $\begin{array}{\|l} 20.632 \\ 1958 \end{array}$ |


| 32 | 0.1 | 80 | Vvtc vy vz 0.7c. x Ro. 80x0.1s result 4.1691.xls | $\begin{aligned} & \hline 6960 \\ & 0249 \\ & 8.6 \end{aligned}$ | $\begin{aligned} & 21198 \\ & 528 \end{aligned}$ | $\begin{array}{\|l} 2119 \\ 8528 \end{array}$ | $\begin{aligned} & 695998 \\ & 662 \end{aligned}$ | $\begin{aligned} & 1674682 \\ & 200 \\ & \hline \end{aligned}$ | $167468$ $2200$ | $\begin{aligned} & 9.6 \mathrm{E}+ \\ & 15 \\ & \hline \end{aligned}$ | $\begin{array}{\|l} 46.1587 \\ 804 \end{array}$ | $\begin{aligned} & 11.664 \\ & 5604 \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 33 | 0.1 | 160 | Vvtc vz vy 0.7c. $x$ Ro yz 6e08 264x0.1s result 2.262125 Good.xls | 6959 <br> 9948 <br> 8.7 | $\begin{aligned} & 64409 \\ & 54.63 \end{aligned}$ | $\begin{array}{\|l\|} \hline 6440 \\ 954.6 \\ 3 \end{array}$ | $\begin{aligned} & 695974 \\ & 356 \end{aligned}$ | $\begin{aligned} & 4975209 \\ & 668 \end{aligned}$ | 497520 9668 | $\begin{aligned} & 2.9 \mathrm{E}+ \\ & 16 \end{aligned}$ | $\begin{array}{\|l} \hline 46.1588 \\ 0458 \end{array}$ | $\begin{aligned} & 21.497 \\ & 8102 \end{aligned}$ |
| 34 | 0.1 | 160 | Vvtc vz vy 0.7c. x yz Ro.1.7e9 $160 \times 0.1$ s result 2.083574 Good.xls | $\begin{aligned} & 6960 \\ & 0037 \\ & 3.5 \end{aligned}$ | $\begin{aligned} & 9.0551 \\ & 0929 \end{aligned}$ | $\begin{aligned} & 9.055 \\ & 1172 \\ & 8 \end{aligned}$ | $\begin{aligned} & 695986 \\ & 887 \end{aligned}$ | $\begin{aligned} & 1674682 \\ & 214 \end{aligned}$ | $167468$ $2214$ | $\begin{aligned} & 9.6 \mathrm{E}+ \\ & 15 \end{aligned}$ | $\begin{array}{\|l\|} \hline 46.1588 \\ 1362 \end{array}$ | $\begin{aligned} & 23.340 \\ & 3664 \end{aligned}$ |
| 35 | 0.1 | $\begin{aligned} & 100 \\ & 0 \end{aligned}$ | Vvtc vz vy 0.7c. $x$ Ro yz 6e08 1000x0.1s result 2.015571 Good.xls | $\begin{aligned} & 6960 \\ & 1216 \\ & 0.8 \end{aligned}$ | $\begin{aligned} & 64349 \\ & 34.11 \end{aligned}$ | $\begin{aligned} & 6434 \\ & 934.1 \\ & 1 \end{aligned}$ | $\begin{aligned} & 695917 \\ & 209 \end{aligned}$ | $\begin{aligned} & 1837268 \\ & 6666 \end{aligned}$ | $1.8373$ $E+10$ | $\begin{aligned} & \text { 1.1E+ } \\ & 17 \end{aligned}$ | $\begin{array}{\|l\|l} \hline 46.1589 \\ 6774 \end{array}$ | $\begin{aligned} & 24.127 \\ & 5284 \end{aligned}$ |
| 36 | 0.1 | $\begin{aligned} & 200 \\ & 0 \end{aligned}$ | Vvtc vz vy 0.7c. $x$ Ro yz 6e08 2000x0.1s result 2.015268 Good.xls | $\begin{aligned} & 6960 \\ & 1216 \\ & 0.8 \end{aligned}$ | $\begin{aligned} & 64349 \\ & 34.11 \end{aligned}$ | $\begin{aligned} & 6434 \\ & 934.1 \\ & 1 \end{aligned}$ | $\begin{aligned} & 695805 \\ & 961 \end{aligned}$ | $\begin{aligned} & 3957120 \\ & 7721 \end{aligned}$ | $\begin{aligned} & 3.9571 \\ & E+10 \end{aligned}$ | $\begin{aligned} & 2.3 \mathrm{E}+ \\ & 17 \end{aligned}$ | $\begin{array}{\|l} \hline 46.1592 \\ 003 \end{array}$ | $\begin{aligned} & 24.131 \\ & 1535 \end{aligned}$ |
| 37 | 0.1 | $\begin{aligned} & 300 \\ & 0 \end{aligned}$ | Vvtc vz vy 0.7c. x Ro yz 6e08 $3000 \times 0.1 \mathrm{~s}$ result 2.015243 Good.xls | $\begin{aligned} & 6960 \\ & 1216 \\ & 0.8 \end{aligned}$ | $\begin{aligned} & 64349 \\ & 34.11 \end{aligned}$ | $\begin{aligned} & 6434 \\ & 934.1 \\ & 1 \end{aligned}$ | $\begin{aligned} & 695694 \\ & 706 \end{aligned}$ | $\begin{aligned} & 6076972 \\ & 8423 \end{aligned}$ | $\begin{aligned} & 6.077 \mathrm{E} \\ & +10 \end{aligned}$ | $\begin{aligned} & 3.5 \mathrm{E}+ \\ & 17 \end{aligned}$ | $\begin{array}{\|l\|} \hline 46.1594 \\ 3289 \end{array}$ | $\begin{aligned} & 24.131 \\ & 4556 \end{aligned}$ |
| 38 | 0.1 | 160 | Vvtc vx vy 0.7c. z 714Ro. 160x0.1s result 0.79744121 extr Good.xls | $\begin{aligned} & 8316 \\ & 096.0 \\ & 02 \end{aligned}$ | $\begin{aligned} & 83160 \\ & 96 \end{aligned}$ | $\begin{aligned} & 4.971 \\ & 4 \mathrm{E}+1 \\ & 1 \end{aligned}$ | $217056$ $5952$ | $\begin{aligned} & 2170565 \\ & 952 \end{aligned}$ | $\begin{aligned} & 4.9714 \\ & E+11 \end{aligned}$ | $\begin{aligned} & 2.85 \mathrm{E} \\ & +18 \end{aligned}$ | $\begin{array}{\|l\|l} 56.5952 \\ 7064 \end{array}$ | $\begin{aligned} & 0.0853 \\ & 7736 \end{aligned}$ |
| 39 | 0.1 | 160 | Vvtc vx vy 0.7c. z Ro. 160x0.1s result 2.104776.xls | $\begin{aligned} & 8316 \\ & 830.0 \\ & 82 \\ & \hline \end{aligned}$ | $\begin{aligned} & 83168 \\ & 30.08 \end{aligned}$ | $\begin{aligned} & 6960 \\ & 0308 \end{aligned}$ $6$ | $217056$ | $\begin{aligned} & 2170567 \\ & 245 \end{aligned}$ | $\begin{aligned} & 695991 \\ & 904 \end{aligned}$ | $\begin{aligned} & 3.99 E \\ & +15 \end{aligned}$ | $\begin{array}{\|l\|l} 56.5952 \\ 7064 \end{array}$ | $\begin{aligned} & 23.104 \\ & 9511 \end{aligned}$ |


| 40 | 0.1 | 228 | Vvtc vx vy 0.7c. z Ro. 160x0.1s result 2.104776.xls | $\begin{aligned} & 8316 \\ & 830.0 \\ & 82 \\ & \hline \end{aligned}$ | $\begin{aligned} & 83168 \\ & 30.08 \end{aligned}$ | $\begin{aligned} & 6960 \\ & 0308 \\ & 6 \end{aligned}$ | $217056$ $7245$ | $\begin{array}{\|l} 2170567 \\ 245 \end{array}$ | $\begin{aligned} & 695991 \\ & 904 \end{aligned}$ | $\begin{array}{\|l} \hline 3.99 E \\ +15 \end{array}$ | $\begin{aligned} & 56.5952 \\ & 7064 \end{aligned}$ | $\begin{aligned} & 23.104 \\ & 9511 \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 41 | 0.1 | 160 | Vvtc vx vy 0.7c. z Ro. 160x0.1s result 2.10477.xls | $\begin{aligned} & 8316 \\ & 830.0 \\ & 82 \\ & \hline \end{aligned}$ | $\begin{aligned} & 83168 \\ & 30.08 \end{aligned}$ | $\begin{aligned} & 6960 \\ & 0308 \\ & 6 \end{aligned}$ | $\begin{aligned} & 217056 \\ & 7245 \end{aligned}$ | $\begin{array}{\|l} 2170567 \\ 245 \end{array}$ | $\begin{aligned} & 695991 \\ & 904 \end{aligned}$ | $\begin{aligned} & 3.99 E \\ & +15 \end{aligned}$ | $\begin{aligned} & 56.5952 \\ & 7064 \end{aligned}$ | $\begin{aligned} & 23.104 \\ & 9511 \end{aligned}$ |
| 42 | 0.1 | 80 | Vvtc vx c. x Ro. $40 \times 0.1 \mathrm{~s}$.result div 0.xls | $\begin{array}{\|l} \hline 7259 \\ 7924 \\ 4.4 \\ \hline \end{array}$ | $\begin{array}{\|l} \hline 6.93 \mathrm{E}- \\ 10 \\ \hline \end{array}$ | $\begin{aligned} & 1.344 \\ & 2 \mathrm{E}-11 \end{aligned}$ | $\begin{aligned} & 186518 \\ & 9527 \end{aligned}$ | $\begin{aligned} & - \\ & 1.05405 \\ & \mathrm{E}-06 \\ & \hline \end{aligned}$ | $\begin{aligned} & 2.0611 \\ & \mathrm{E}-08 \end{aligned}$ | $0.1180$ $9$ | $\begin{aligned} & 78.4047 \\ & 2937 \end{aligned}$ | 0 |
| 43 | 0.1 | 40 | Vvtc vx vz eq .7c.x eq 2c 40 x .1 s result 171.14.xls | $\begin{aligned} & 6207 \\ & 8344 \\ & 3.5 \end{aligned}$ | $\begin{aligned} & 6.9306 \\ & \mathrm{E}-10 \end{aligned}$ | $\begin{aligned} & 7171 \\ & 9852 \\ & 7 \end{aligned}$ | $\begin{aligned} & 142632 \\ & 7053 \end{aligned}$ | $\begin{aligned} & 1.05421 \\ & \text { E-06 } \end{aligned}$ | $\begin{aligned} & 152274 \\ & 2080 \end{aligned}$ | $\begin{array}{\|l} 8.72 \mathrm{E} \\ +15 \end{array}$ | $\begin{aligned} & 81.8282 \\ & 9177 \end{aligned}$ | $\begin{array}{\|l} 0.2831 \\ 6468 \end{array}$ |
| 44 | 0.1 | 80 | Vvtc vz -c. x Ro. $80 \times 0.1 \mathrm{~s}$ result PI see.xls | $\begin{array}{\|l\|} \hline 6959 \\ 9999 \\ 8.6 \\ \hline \end{array}$ | 6.93E- $10$ | $\begin{aligned} & 2997 \\ & 9245 . \\ & 8 \end{aligned}$ | $\begin{aligned} & 695996 \\ & 162 \end{aligned}$ | $\begin{array}{\|l} 4.32552 \\ E-06 \end{array}$ | $\begin{aligned} & 236835 \\ & 8279 \end{aligned}$ | $\begin{aligned} & 1.36 \mathrm{E} \\ & +16 \end{aligned}$ | $\begin{aligned} & 89.9988 \\ & 8233 \end{aligned}$ | $\begin{aligned} & 11.664 \\ & 5604 \end{aligned}$ |
| 45 | 0.1 | 160 | Vvtc vx vyO vz c. z4.97e11 Ro. 160x0.1s result div0.xls | $\begin{array}{\|l} 6.697 \\ 38 \mathrm{E}- \\ 06 \end{array}$ | $\begin{aligned} & 1.3131 \\ & \mathrm{E}-05 \end{aligned}$ | $\begin{aligned} & 4.923 \\ & 4 \mathrm{E}+1 \\ & 1 \end{aligned}$ | $\begin{aligned} & 6.6138 \\ & \text { E-06 } \end{aligned}$ | $\begin{aligned} & 1.29672 \\ & \text { E-05 } \end{aligned}$ | $\begin{aligned} & 4.9237 \\ & E+11 \end{aligned}$ | $\begin{aligned} & 2.82 \mathrm{E} \\ & +18 \end{aligned}$ | $\begin{aligned} & 90.0011 \\ & 1767 \end{aligned}$ | 0 |
| 46 | 0.1 | 160 | Vvtc vz c-c. y <br> Ro. 160x0.1s <br> result <br> $2.08388 . x$ s | $\begin{aligned} & 3.842 \\ & 59 \mathrm{E}- \\ & 06 \end{aligned}$ | $\begin{aligned} & 69600 \\ & 6966 \end{aligned}$ | $\begin{aligned} & 1658 \\ & 889.8 \\ & 6 \end{aligned}$ | $\begin{aligned} & 1.5185 \\ & \mathrm{E}-05 \end{aligned}$ | $\begin{aligned} & 6959984 \\ & 10 \end{aligned}$ | $\begin{aligned} & 236670 \\ & 3025 \end{aligned}$ | $\begin{array}{\|l} 1.4 \mathrm{E}+ \\ 16 \end{array}$ | $\begin{aligned} & 90.0011 \\ & 1767 \end{aligned}$ | $\begin{array}{\|l} 23.339 \\ 898 \end{array}$ |
| 47 | 0.1 | 80 | Vvtc vz C-c. y <br> Ro. 80x0.1s <br> result <br> $2.320042 . x l \mathrm{~s}$ | $\begin{aligned} & 9.825 \\ & 82 \mathrm{E}- \\ & 07 \end{aligned}$ | $\begin{array}{\|l} 69600 \\ 0777 \end{array}$ | $\begin{aligned} & 1247 . \\ & 0530 \\ & 5 \end{aligned}$ | $\begin{aligned} & 3.7712 \\ & \mathrm{E}-06 \end{aligned}$ | $\begin{aligned} & 6959972 \\ & 41.8 \end{aligned}$ | $116919$ $2521$ | $\begin{array}{\|l} 6.7 \mathrm{E}+ \\ 15 \end{array}$ | $\begin{aligned} & 90.0011 \\ & 1767 \end{aligned}$ | $\begin{aligned} & 20.961 \\ & 1428 \end{aligned}$ |
| 48 | 0.1 | 160 | Vvtc vz c-c. y Ro. 160x0.1s result $2.083588 . x$ s | $\begin{aligned} & 6960 \\ & 0696 \\ & 5.5 \end{aligned}$ | $\begin{array}{\|l} 4.4364 \\ \text { E-06 } \end{array}$ | $\begin{aligned} & 1658 \\ & 889.8 \\ & 6 \end{aligned}$ | $\begin{aligned} & 695998 \\ & 410 \end{aligned}$ | $\begin{aligned} & - \\ & 1.75225 \\ & \mathrm{E}-05 \end{aligned}$ | $236670$ $3025$ | $\begin{array}{\|l} 1.4 \mathrm{E}+ \\ 16 \end{array}$ | $\begin{aligned} & 90.0011 \\ & 1767 \end{aligned}$ | $\begin{aligned} & 23.339 \\ & 898 \end{aligned}$ |
| 49 | 0.1 | 80 | Vvtc vz c. x Ro. $80 \times 0.1 \mathrm{~s}$ result 4.1067.xls | $\begin{aligned} & 6959 \\ & 9999 \\ & 8.6 \end{aligned}$ | $\begin{aligned} & 6.93 \mathrm{E}- \\ & 10 \end{aligned}$ | $\begin{aligned} & 2997 \\ & 9245 . \\ & 8 \\ & \hline \end{aligned}$ | $\begin{aligned} & 695996 \\ & 162 \end{aligned}$ | $\begin{array}{\|l} 4.32475 \\ E-06 \end{array}$ | $\begin{aligned} & 236835 \\ & 8279 \end{aligned}$ | $\begin{aligned} & 1.4 \mathrm{E}+ \\ & 16 \end{aligned}$ | $\begin{aligned} & 90.0011 \\ & 1767 \end{aligned}$ | $\begin{aligned} & 11.664 \\ & 5604 \end{aligned}$ |


| 50 | 0.1 | 40 | Vvtc $40 \times 0.1 \mathrm{~s}$ Y NORMAL light ray in different direction result 2.5.xls | $\begin{aligned} & 5995 \\ & 8443 \\ & 0.5 \end{aligned}$ | $\begin{aligned} & 3.6662 \\ & \mathrm{E}-07 \end{aligned}$ | $\begin{aligned} & 6477 \\ & 007.4 \end{aligned}$ | $\begin{aligned} & 599583 \\ & 146 \end{aligned}$ | $\begin{array}{\|l} \hline 1.0541 E \\ -06 \end{array}$ | $473191$ $257$ | $\begin{aligned} & 2.7 \mathrm{E}+ \\ & 15 \end{aligned}$ | $\begin{aligned} & 90.0011 \\ & 1767 \end{aligned}$ | $\begin{aligned} & 19.431 \\ & 5581 \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 51 | 0.1 | 40 | Vvtc vz eq c.x   <br> eq $2 c$  <br> 40x.1sresult   <br> 2.502.xls   <br>    <br>    | $\begin{aligned} & 5995 \\ & 8443 \\ & 0.5 \end{aligned}$ | $\begin{aligned} & 3.6662 \\ & \mathrm{E}-07 \end{aligned}$ | $\begin{aligned} & 6477 \\ & 007.4 \end{aligned}$ | $\begin{aligned} & 599583 \\ & 146 \end{aligned}$ | $\begin{array}{\|l} \hline 1.0541 E \\ -06 \end{array}$ | $\begin{array}{\|l\|} 473191 \\ 257 \end{array}$ | $\begin{aligned} & 2.7 \mathrm{E}+ \\ & 15 \end{aligned}$ | $\begin{aligned} & 90.0011 \\ & 1767 \end{aligned}$ | $\begin{aligned} & 19.431 \\ & 5581 \end{aligned}$ |
| 52 | 0.1 | 160 | Vvtc vz vy 0.7c. x Ro. 160x0.1s result 15.32195 not bad.xls | $\begin{aligned} & 6510 \\ & 3513 \\ & 0.2 \end{aligned}$ | $\begin{aligned} & 23237 \\ & 90014 \end{aligned}$ | $\begin{aligned} & 1741 \\ & 6368 \\ & 0 \\ & \hline \end{aligned}$ | $\begin{aligned} & 495671 \\ & 353 \end{aligned}$ | $\begin{array}{\|l} 2323788 \\ 188 \end{array}$ | 461533 6694 | $\begin{array}{\|l} 2.6 \mathrm{E}+ \\ 16 \end{array}$ | $\begin{aligned} & 92.8813 \\ & 6738 \end{aligned}$ | $\begin{array}{\|l} 3.1739 \\ 2578 \end{array}$ |
| 53 | 0.1 | $\begin{aligned} & 100 \\ & 0 \end{aligned}$ | Vvtc vz 0.25c.vx 0.97c, yRo. x $2 e 8$ z 6,5e8 1000x0.1s result 2.3576 Good.xls | $\begin{aligned} & 3511 \\ & 4073 . \\ & 22 \end{aligned}$ | $\begin{aligned} & 69599 \\ & 9620 \end{aligned}$ | $\begin{aligned} & 1234 \\ & 7120 . \\ & 7 \end{aligned}$ | $\begin{aligned} & 728731 \\ & 1867 \end{aligned}$ | $\begin{aligned} & 6958953 \\ & 09.6 \end{aligned}$ | $\begin{aligned} & 2.8347 \\ & \mathrm{E}+10 \end{aligned}$ | $\begin{aligned} & 1.6 \mathrm{E}+ \\ & 17 \end{aligned}$ | $\begin{aligned} & 92.8813 \\ & 6738 \end{aligned}$ | $\begin{aligned} & 20.626 \\ & 5423 \end{aligned}$ |
| 54 | 0.1 | 160 | Vvtc vz $0.25 c . v x$ <br> $0.97 c$, $y R o r$ x <br> $2 e 8$ $z$ $6,5 e 8$ <br> $160 \times 0.1 s$ result  <br> 2.377165   <br> Good.xls   | $\begin{aligned} & 2761 \\ & 9255 . \\ & 29 \end{aligned}$ | $\begin{aligned} & 69599 \\ & 9577 \end{aligned}$ | $\begin{aligned} & 1668 \\ & 0176 . \\ & 8 \end{aligned}$ | $991675$ <br> 061 | $\begin{aligned} & 6959862 \\ & 05.8 \end{aligned}$ | $396438$ <br> 7731 | $\begin{aligned} & 2.3 E+ \\ & 16 \end{aligned}$ | $\begin{aligned} & 92.8813 \\ & 6738 \end{aligned}$ | $\begin{aligned} & 20.457 \\ & 457 \end{aligned}$ |
| 55 | 0.1 | 160 | Vvtc vz 0.25c.vx 0.97c, yRo. x 1.8 e 8 z 6,2e8 160x0.1s result 240159 <br> Good.xls | $\begin{aligned} & 1511 \\ & 4079 . \\ & 8 \end{aligned}$ | $\begin{aligned} & 69599 \\ & 9597 \end{aligned}$ | $\begin{aligned} & 1765 \\ & 2877 . \\ & 1 \end{aligned}$ | $101167$ <br> 4778 | $\begin{aligned} & 6959862 \\ & 46.4 \end{aligned}$ | $399438$ <br> 7580 | $\begin{aligned} & 2.3 \mathrm{E}+ \\ & 16 \end{aligned}$ | $\begin{array}{\|l\|} \hline 92.8813 \\ 6738 \end{array}$ | $\begin{aligned} & 20.249 \\ & 7399 \end{aligned}$ |
| 56 | 0.1 | 160 | Vvtc vz 0.25c.vx 0.97c, yRo. x 1.5 e 8 z 5.8 e 8 160x0.1s result 2. Good.xls | $\begin{aligned} & 1037 \\ & 23.40 \\ & 16 \end{aligned}$ | $\begin{aligned} & 69599 \\ & 9651 \end{aligned}$ | $\begin{aligned} & 4017 \\ & 19.00 \\ & 9 \end{aligned}$ | $104167$ $4338$ | $\begin{aligned} & 6959863 \\ & 40.5 \end{aligned}$ | $\begin{array}{\|l} 403438 \\ 7381 \end{array}$ | $\begin{aligned} & 2.3 \mathrm{E}+ \\ & 16 \end{aligned}$ | $\begin{aligned} & 92.8813 \\ & 6738 \end{aligned}$ | $\begin{aligned} & 19.928 \\ & 0719 \end{aligned}$ |
| 57 | 0.1 | 160 | Vvtc vz 0.25c.vx 0.97c, yRo. 160x0.1s result | $\begin{aligned} & 4201 \\ & 2429 \\ & 4.9 \end{aligned}$ | $\begin{aligned} & 69599 \\ & 9699 \end{aligned}$ | $9665$ $4868 .$ | $591680$ $288$ | $\begin{array}{\|l} \hline 6959904 \\ 80.2 \end{array}$ | 401533 <br> 4352 | $\begin{aligned} & 2.3 \mathrm{E}+ \\ & 16 \end{aligned}$ | $\begin{aligned} & 92.8813 \\ & 6738 \end{aligned}$ | $\begin{aligned} & 17.014 \\ & 3186 \end{aligned}$ |


|  |  |  | 2.85844.xls |  |  | 3 |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 58 | 0.1 | 80 | Vvtc vx 0.25c.vz 0.97c, y Ro. $80 \times 0.1 \mathrm{~s}$ result 4.297657.xls | $\begin{aligned} & 2995 \\ & 8484 \\ & 3.5 \end{aligned}$ | $\begin{aligned} & 69600 \\ & 2951 \end{aligned}$ | $\begin{aligned} & 1606 \\ & 142.3 \\ & 4 \end{aligned}$ | $292090$ $044$ | $\begin{aligned} & 6960030 \\ & 05.3 \end{aligned}$ | $\begin{array}{\|l} 306334 \\ 67.4 \end{array}$ | $\begin{aligned} & 1.76 E \\ & +14 \end{aligned}$ | $\begin{aligned} & 92.8813 \\ & 6738 \end{aligned}$ | $\begin{aligned} & 11.315 \\ & 6416 \end{aligned}$ |
| 59 | 0.1 | 80 | Vvtc vx 0.25c.vz 0.97c, y Ro. $80 \times 0.1 \mathrm{~s}$ result 4.16899.xls | $\begin{aligned} & 7494 \\ & 811.4 \\ & 5 \end{aligned}$ | $\begin{aligned} & 69599 \\ & 9999 \end{aligned}$ | $\begin{aligned} & 2902 \\ & 7280 . \\ & 1 \end{aligned}$ | $\begin{aligned} & 592089 \\ & 570 \end{aligned}$ | $\begin{aligned} & 6959976 \\ & 53.7 \end{aligned}$ | $229315$ $3054$ | $\begin{aligned} & 1.3 \mathrm{E}+ \\ & 16 \end{aligned}$ | $\begin{aligned} & 92.8813 \\ & 6738 \end{aligned}$ | $\begin{aligned} & 11.664 \\ & 8728 \end{aligned}$ |
| 60 | 0.1 | 80 | Vvtc vx 0.25c.vz 0.97c, y less Ro. $160 \times 0.1 \mathrm{~s}$ result 2.08335.x\|s | $\begin{aligned} & 908.0 \\ & 5550 \\ & 36 \end{aligned}$ | $\begin{aligned} & 69600 \\ & 2962 \end{aligned}$ | $\begin{aligned} & 3516 . \\ & 8838 \\ & 6 \end{aligned}$ | $\begin{aligned} & 592091 \\ & 386 \end{aligned}$ | $\begin{aligned} & 6959944 \\ & 03.7 \end{aligned}$ | $229316$ $0088$ | $\begin{aligned} & 1.3 \mathrm{E}+ \\ & 16 \end{aligned}$ | $\begin{aligned} & 92.8813 \\ & 6738 \end{aligned}$ | $\begin{aligned} & 23.340 \\ & 5226 \end{aligned}$ |
| 61 | 0.1 | 80 | Vvtc vx 0.25c.vz 0.97 c, y less Ro. $80 \times 0.1 \mathrm{~s}$ result 4.16899.xls | $\begin{aligned} & 7494 \\ & 811.4 \\ & 5 \end{aligned}$ | $\begin{aligned} & 69599 \\ & 9999 \end{aligned}$ | $\begin{aligned} & 2902 \\ & 7280 . \\ & 1 \end{aligned}$ | $\begin{aligned} & 592089 \\ & 570 \end{aligned}$ | $\begin{aligned} & 6959961 \\ & 61.6 \end{aligned}$ | $229315$ $3054$ | $\begin{aligned} & 1.3 \mathrm{E}+ \\ & 16 \end{aligned}$ | $\begin{aligned} & 92.8813 \\ & 6738 \end{aligned}$ | $\begin{array}{\|l\|} 11.664 \\ 8728 \end{array}$ |
| 62 | 0.1 | $\begin{aligned} & 200 \\ & 0 \end{aligned}$ | Vvtc vz 0.25c.vx 0.97c, yRo. x $2 e 8$ z 6,5e8 $2000 \times 0.1$ s result 2.36 Good.xls | $\begin{aligned} & 2761 \\ & 9255 . \\ & 29 \end{aligned}$ | $\begin{aligned} & 69599 \\ & 9577 \end{aligned}$ | $\begin{aligned} & 1668 \\ & 0176 . \\ & 8 \end{aligned}$ | $\begin{aligned} & 1.4782 \\ & E+10 \end{aligned}$ | $\begin{aligned} & 6957869 \\ & 80.5 \end{aligned}$ | $\begin{aligned} & 5.7375 \\ & \mathrm{E}+10 \end{aligned}$ | $\begin{aligned} & 3.3 \mathrm{E}+ \\ & 17 \end{aligned}$ | $\begin{aligned} & 92.8818 \\ & 9979 \end{aligned}$ | $\begin{aligned} & 20.629 \\ & 1925 \end{aligned}$ |
| 63 | 0.1 | 40 | Vvtc -vx vz eq .7c.x eq 2c 40x.1s result 7.217.xls | $\begin{aligned} & 5783 \\ & 8638 \end{aligned}$ $7.5$ | $\begin{aligned} & 6.9306 \\ & \mathrm{E}-10 \end{aligned}$ | $\begin{aligned} & 7171 \\ & 9852 \\ & 7 \end{aligned}$ | 227158 051 | $\begin{aligned} & 1.05418 \\ & \text { E-06 } \end{aligned}$ | $\begin{aligned} & 152274 \\ & 1731 \end{aligned}$ | $\begin{aligned} & 8.72 \mathrm{E} \\ & +15 \end{aligned}$ | $\begin{aligned} & 98.1701 \\ & 1138 \end{aligned}$ | $\begin{aligned} & 6.7383 \\ & 2433 \end{aligned}$ |
| 64 | 0.1 | 40 | Vvtc vz vz eq .7c.x eq 2c 40x. 1 sresult 7.127.xls | $\begin{aligned} & 5783 \\ & 8638 \end{aligned}$ $7.5$ | $6.9306$ <br> E-10 | $\begin{aligned} & 7171 \\ & 9852 \\ & 7 \end{aligned}$ | 227158 051 | $\begin{aligned} & - \\ & 1.05418 \\ & \mathrm{E}-06 \end{aligned}$ | $\begin{aligned} & 152274 \\ & 1731 \end{aligned}$ | $\begin{aligned} & 8.72 \mathrm{E} \\ & +15 \end{aligned}$ | $\begin{aligned} & 98.1701 \\ & 1138 \end{aligned}$ | $\begin{aligned} & 6.7383 \\ & 2433 \end{aligned}$ |
| 65 | 0.1 | 80 | Vvtc vy vz 0.7c. $x$ Ro. $80 \times 0.1 \mathrm{~s}$ result 4.169.xls | 2119 <br> 8528 | $\begin{aligned} & 69600 \\ & 1491 \end{aligned}$ | 2119 <br> 8528 | $167468$ $2200$ | $\begin{aligned} & 6959976 \\ & 53.7 \end{aligned}$ | $167468$ $2200$ | $\begin{aligned} & 9.6 \mathrm{E}+ \\ & 15 \\ & \hline \end{aligned}$ | $\begin{aligned} & 98.1717 \\ & 0823 \end{aligned}$ | $\begin{aligned} & 11.664 \\ & 5604 \end{aligned}$ |


| 66 | 0.1 | 160 | Vvtc vx vz 0.7c. y Ro. 160x0.1s result 2.10471.xls | $\begin{array}{\|l} 7078 \\ 6889 \\ 8.4 \\ \hline \end{array}$ | $\begin{aligned} & 69600 \\ & 0057 \end{aligned}$ | $\begin{array}{\|l} 7078 \\ 6889 \\ 8 \\ \hline \end{array}$ | $\begin{aligned} & 217056 \\ & 7245 \end{aligned}$ | $\begin{aligned} & 6959919 \\ & 03.9 \end{aligned}$ | $217056$ <br> 7245 | $\begin{aligned} & 1.2 \mathrm{E}+ \\ & 16 \end{aligned}$ | $\begin{aligned} & 98.1717 \\ & 0823 \end{aligned}$ | $\begin{aligned} & 23.104 \\ & 7933 \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 67 | 0.1 | 80 | Vvtc vz 0.25c.vx 0.97c, y Ro. $80 \times 0.1 \mathrm{~s}$ result 4.3715.xls | $\begin{array}{\|l\|} 1606 \\ 213.1 \\ 98 \end{array}$ | $\begin{aligned} & 69600 \\ & 2966 \end{aligned}$ | $\begin{array}{\|l} 4147 \\ 22.46 \\ 3 \end{array}$ | $\begin{array}{\|l\|l} 306335 \\ 37.7 \end{array}$ | $\begin{aligned} & 6960030 \\ & 23.8 \end{aligned}$ | $\begin{aligned} & 790954 \\ & 5.39 \end{aligned}$ | $\begin{array}{\|l} 4.53 E \\ +13 \end{array}$ | $\begin{aligned} & 101.222 \\ & 4936 \end{aligned}$ | $\begin{aligned} & 11.124 \\ & 3135 \end{aligned}$ |
| 68 | 0.1 | 80 | Vvtc vz 0.25c.vx 0.97c, y Ro. 80x0.1s result 4.169.x\|s | $\begin{aligned} & 2902 \\ & 7280 . \\ & 06 \end{aligned}$ | $\begin{aligned} & 69600 \\ & 1491 \end{aligned}$ | $\begin{aligned} & 7494 \\ & 811.4 \\ & 5 \end{aligned}$ | $229315$ $3054$ | $\begin{aligned} & 6959976 \\ & 53.7 \end{aligned}$ | $\begin{aligned} & 592089 \\ & 570 \end{aligned}$ | $\begin{aligned} & 3.4 \mathrm{E}+ \\ & 15 \end{aligned}$ | $\begin{aligned} & 101.222 \\ & 4936 \end{aligned}$ | $\begin{array}{\|l\|} 11.664 \\ 8728 \end{array}$ |
| 69 | 0.1 | 160 | Vvtc vz 0.25c.vx 0.97c, y less Ro. 160x0.1s result 2.083537.xls | $\begin{array}{\|l} 3516 . \\ 8838 \\ 55 \end{array}$ | $\begin{aligned} & 69600 \\ & 2962 \end{aligned}$ | $\begin{array}{\|l} - \\ 908.0 \\ 5550 \\ 8 \end{array}$ | $229316$ $0088$ | $\begin{aligned} & 6959944 \\ & 03.7 \end{aligned}$ | $\begin{aligned} & 592091 \\ & 386 \end{aligned}$ | $\begin{array}{\|l} 3.4 \mathrm{E}+ \\ 15 \end{array}$ | $\begin{aligned} & 101.222 \\ & 4936 \end{aligned}$ | $\begin{aligned} & 23.340 \\ & 3664 \end{aligned}$ |
| 70 | 0.1 | 80 | Vvtc vx c-c. z Ro. $80 \times 0.1 \mathrm{~s}$ result 2.3200.xIs | $\begin{aligned} & 1247 . \\ & 0530 \\ & 45 \\ & \hline \end{aligned}$ | $\begin{array}{\|l} - \\ 1.0874 \\ \mathrm{E}-06 \end{array}$ | $\begin{aligned} & 6960 \\ & 0077 \\ & 7 \end{aligned}$ | $116919$ $2521$ | $\begin{aligned} & 4.30388 \\ & \text { E-06 } \end{aligned}$ | $\begin{aligned} & 695997 \\ & 242 \end{aligned}$ | $\begin{array}{\|l} \hline 3.99 E \\ +15 \end{array}$ | $\begin{aligned} & 101.595 \\ & 2706 \end{aligned}$ | $\begin{aligned} & 20.960 \\ & 969 \end{aligned}$ |
| 71 | 0.1 | 160 | Vvtc vx c-c. y Ro.2.4e in $z$ $160 \times 0.1 \mathrm{~s}$ result 16.2.xls | $\begin{aligned} & 2997 \\ & 9245 . \\ & 8 \end{aligned}$ | $\begin{array}{\|l\|} \hline 69600 \\ 8000 \end{array}$ | $\begin{aligned} & 2400 \\ & 0000 \\ & 00 \end{aligned}$ | $476669$ $9340$ | $\begin{aligned} & 6960075 \\ & 22.9 \end{aligned}$ | $\begin{aligned} & 239999 \\ & 8355 \end{aligned}$ | $\begin{array}{\|l} 1.38 \mathrm{E} \\ +16 \end{array}$ | $\begin{aligned} & 101.595 \\ & 2706 \end{aligned}$ | $\begin{aligned} & 3.0003 \\ & 7974 \end{aligned}$ |
| 72 | 0.1 | 160 | Vvtc vx c-c. $y$ Ro.2.4e in $\quad$ x $160 \times 0.1 \mathrm{~s}$ result $2.083588 . x l \mathrm{~s}$ | $\begin{aligned} & 1658 \\ & 889.8 \end{aligned}$ $57$ | $\begin{aligned} & 69600 \\ & 6966 \end{aligned}$ | $\begin{aligned} & 8.814 \\ & 9 \mathrm{E}-08 \end{aligned}$ | $236670$ $3025$ | $\begin{aligned} & 6959984 \\ & 10 \end{aligned}$ | $\begin{aligned} & 3.4244 \\ & \mathrm{E}-07 \end{aligned}$ | $1.9620$ | $\begin{aligned} & 101.595 \\ & 2706 \end{aligned}$ | $\begin{aligned} & 23.339 \\ & 898 \end{aligned}$ |
| 73 | 0.1 | 40 | Vvtc vy vz eq .7c.x eq 2c 40x result 12.032.1s.xls | $\begin{aligned} & 5995 \\ & 8491 \\ & 5.5 \end{aligned}$ | $\begin{aligned} & 21198 \\ & 528 \end{aligned}$ | $\begin{aligned} & 7171 \\ & 9852 \\ & 7 \end{aligned}$ | $\begin{aligned} & 599584 \\ & 480 \end{aligned}$ | $\begin{aligned} & 8267424 \\ & 60.5 \end{aligned}$ | $\begin{aligned} & 152274 \\ & 1954 \end{aligned}$ | $\begin{array}{\|l} 8.72 \mathrm{E} \\ +15 \end{array}$ | $\begin{aligned} & 133.841 \\ & 2196 \end{aligned}$ | $\begin{aligned} & 4.0416 \\ & 9627 \end{aligned}$ |
| 74 | 0.1 | 80 | Vvtc vx 0.25c.vz 0.97c, y 3000 Ro. 80x0.1s result <br> 4.169102.xls | $\begin{array}{\|l} 7494 \\ 811.4 \\ 5 \end{array}$ | $\begin{aligned} & 69600 \\ & 2999 \end{aligned}$ | $\begin{aligned} & 2902 \\ & 7280 . \\ & 1 \end{aligned}$ | $\begin{array}{\|l\|} \hline- \\ 592089 \\ 570 \end{array}$ | $\begin{aligned} & 6959991 \\ & 61.6 \end{aligned}$ | $229315$ $3054$ | $\begin{aligned} & 1.3 \mathrm{E}+ \\ & 16 \end{aligned}$ | $\begin{aligned} & 168.404 \\ & 7293 \end{aligned}$ | $\begin{aligned} & 11.664 \\ & 5604 \end{aligned}$ |


| 75 | 0.1 | 40 | Vvtc vy c. x Ro. 40x0.1s result 4.65524.xls | $\begin{aligned} & 6959 \\ & 9999 \\ & 8.6 \end{aligned}$ | $\begin{aligned} & 29979 \\ & 245.8 \end{aligned}$ | $1.344$ $2 \mathrm{E}-11$ | $\begin{aligned} & 695998 \\ & 564 \end{aligned}$ | $\begin{aligned} & 1169190 \\ & 027 \end{aligned}$ | $\begin{aligned} & 2.0491 \\ & \text { E-08 } \end{aligned}$ | $\begin{aligned} & 0.1174 \\ & 1 \end{aligned}$ | $\begin{aligned} & 168.404 \\ & 7293 \end{aligned}$ | $\begin{aligned} & 10.446 \\ & 4361 \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 76 | 0.1 | 20 | vak variable time create vak1 20x 0.1 sec result 9.956.xls | $\begin{aligned} & 6959 \\ & 9988 \\ & 1.5 \end{aligned}$ | $\begin{aligned} & 35.571 \\ & 8466 \end{aligned}$ | $\begin{aligned} & 1.342 \\ & 5 \mathrm{E}-09 \end{aligned}$ | $\begin{aligned} & 695999 \\ & 990 \end{aligned}$ | $\begin{aligned} & 2098547 \\ & 16.6 \end{aligned}$ | $\begin{aligned} & 1.2078 \\ & E-10 \end{aligned}$ | $\begin{aligned} & - \\ & 0.0006 \\ & 9 \end{aligned}$ | $\begin{aligned} & 168.404 \\ & 7293 \end{aligned}$ | $\begin{aligned} & 4.8844 \\ & 5089 \end{aligned}$ |

Table 2. The various filenames, Time step values, Number of iterations, initial position, and final position of the Neutrino, General relativistic deflection (bending) angle, Calculated Solar elongation angle in degrees, and SITA Deflection are mentioned there.

